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Fracture evolution in concrete compressive fatigue experiments based on X-ray micro-CT images

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Abstract

This study examines the fatigue performance of plain concrete specimens under uniaxial compression. The experimental program was developed for investigating the fracture evolution in concrete cubic specimens subjected to cyclic compression using the advanced X-ray micro-computed tomography system SkyScan 1173. As compared to other experiments, the 3D micro-CT damage images were shown for a various number of loading cycles. The quantitative evolution of the cracking volume with increasing damage revealed a strongly non-linear shape. The increase of the total crack volume was higher by 30% as compared to the monotonic fatigue test.

Keywords: micro-CT; plain concrete; compression; fatigue; fracture; meso-structure

1. Introduction

Fatigue is a process of progressive and permanent structural damage in materials which are subjected to repeatedly applied stresses and strains. As a result, macro-cracks or complete fracture occur after a certain number of repeated loading. The knowledge on the concrete behaviour in fatigue is essential for describing the behaviour of different engineering structures under repeated loads with random and varying amplitudes (e.g. concrete bridge desks, highway pavements, railway slab tracks, crane beams, wind power tower bases). The concrete fatigue is still a challenging topic in research works. In particular, the knowledge on the effect of cyclic loading on the evolution of fracture (crack initiation and growth, crack pattern, crack shape, crack number etc.) is still very limited in spite of many laboratory tests (e.g. [1-10]). This problem is also difficult since fatigue displacements and strains are subjected to a pronounced statistical scatter [11]. The progressive decreasing of the compression strength of concrete under cyclic loads happens due to internal damage. The fatigue test results on concrete in compression (mainly low and medium-cycle results) are usually described with the aid of the so-called Wöhler-curve or S-N curve ([2], [12-16]), that shows a linear relationship between the logarithm of the cycles' number

and maximum fraction of the monotonic compressive strength. There exist several factors that affect concrete fatigue behaviour. The fatigue strength mainly depends on the maximum and minimum stress in the cycle (often identified as the live load and dead load). An increase of the minimum stress and a decrease of the maximum stress level result in the increased fatigue strength for a given number of cycles. The frequency between 1 and 15 Hz has a little effect on the fatigue strength provided that the maximum stress is lower than about 75% of the monotonic strength. At higher stresses, the fatigue strength decreases with decreasing frequency ([16, 17]). The fatigue strength is also affected by water-cement ratio, cement content, amount of entrained air, concrete class, rest periods, curing conditions and age during loading [13]. It is assumed that damage linearly increases with the number of cycles applied at a certain stress level [17]. The strain at the concrete failure during fatigue tests corresponds to that at the peak load during quasi-static tests [18]. The failure meso-mechanism in concrete in fatigue compressive tests is almost the same as in monotonic compressive tests [19].

The presented research work is experimentally oriented. It is aimed at quantitative investigations of a three-dimensional (3D) crack evolution in plain concrete under uniaxial fatigue compression loading with very advanced non-destructive X-ray micro-computed tomography system SkyScan 1173 [20]. Micro-computed tomography (in short 'micro-CT') is a 3D imaging technique that uses X-rays to see the interior of different materials [21]. The micro-CT device performs 2D planar X-ray images and reconstructs the data into 2D cross-sectional slices that are further processed to obtain a full 3D image. Thus the volumetric information about changes in the internal micro/meso-structure may be achieved. In the paper, attention was focused on changes in the fracture volume with an increasing number of loading cycles in concrete compressive fatigue experiments. This knowledge is important to better understand a fracture process for enhancing the fatigue life of concrete members and structures. Our tomography system SkyScan 1173 was already successfully used for observations of a 3D fracture process inside concrete during different quasi-static monotonic tests: bending [22], uniaxial compression [23], tension splitting [24] and wedge splitting [25]. The micro-CT images of the concrete structure allowed us next for developing a very effective numerical 3D four-phase concrete model (composed of aggregate, cement matrix, macro-pores and interfacial transitional zones (ITZs)) within the discrete mechanics [23, 24, 26, 27] and continuum mechanics [22, 28, 29] to realistically reproduce strength, brittleness and fracture in plain concrete in different tests.

The novel elements of the current paper on concrete fatigue in compression are: 1) the full 3D damage maps with high-resolution of fractured concrete specimens for the different number of loading cycles in fatigue compression by considering concrete meso-structure (aggregate, cement matrix and pores) and 2) the quantitative estimation of changes of the cracks' and pores' volume (based on 3D damage maps)

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with increasing cycle number and damage. Our experimental results may create a solid comparative basis for numerical calculations using different fatigue continuum models for concrete based on fracture/damage mechanics (e.g. [30-34]) or discrete mechanics ([35]). The micro-CT studies were also carried out for steel fiber-reinforced concrete under low cycle fatigue in uniaxial compression by Vicente et al. [19] that indicated a similar crack pattern in specimens under monotonic and cyclic loads. However, the 2D images of concrete specimens were shown only and the micro-CT scans were solely made at the beginning and end of tests. The micro-CT technique was also used in fatigue loading tests for scanning of other engineering materials ([36, 37]). To our knowledge, 3D micro-CT scans of concrete specimens at different loading cycles in fatigue compression have not been performed yet.

2. Specimen preparation, experimental set-up and distribution of pores

Specimen preparation

The laboratory fatigue experiments on concrete in uniaxial compression were carried out at the Gdansk University of Technology. The concrete specimens were composed of an ordinary Portland cement (CEM I 32.5 R), sand and gravel particles and water. The round-shape sand and gravel particles were used with the maximum diameter of d_{max}=16 mm, mean diameter of d_{50}=2 mm and particle volume of β=75% (Figure 1). The water/cement ratio was fixed to 0.42. The composition of the concrete mix was described in Table 1. A small super plasticizer quantity was used to improve the workability of the fresh concrete. The tests were carried out on relatively small concrete cubes of 40×40×40 mm^3 to obtain a very high resolution of 3D micro-CT images of fractured concrete specimens. The cubes were cut out from the same concrete block of the size 500×500×200 mm^3 after the seventh day. The concrete block was covered with a plastic sheet during the initial curing period to avoid the surface evaporation and autogenous shrinkage. They were next kept for 28 days in water. The uniaxial compressive strength f_c was measured on three cube concrete specimens 10×10×10 cm^3 and Young's modulus E and Poisson's ratio υ were determined on three cylindrical concrete specimens 15×30 cm^2. The mean measured values were: f_c=51.81 MPa with the standard deviation of 3.36 MPa, E=36.1 GPa with the standard deviation of 2.29 GPa and υ=0.22 with the standard deviation of 0.03. The mean tensile strength during three-point bending on three concrete specimens 4×4×16 cm^2 was 4.04 MPa. The monotonic and fatigue tests were conducted using the servo-hydraulic machine Zwick Roell HB250 (Figure 2) with the maximum loading capacity of 250 kN and maximum frequency of 15 Hz. The machine was equipped with two compressive steel plates and the cubes were always loaded along the casting direction (vertical axis). A sinusoidal vertical force was applied along the top boundary in fatigue tests. The vertical force F and the axial displacement u were continuously monitored and recorded. Initially, a monotonic test was carried out with the controlled vertical displacement rate of 0.002 mm/min. The mean maximum vertical force was

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F_{max}=81 kN that results in the uniaxial compressive strength of f_c=51.5 MPa which was almost equal to the experimental results for the concrete specimens of 100×100×100 mm^3. Thus the size effect on the nominal strength was negligible in the tests. However, the size effect on the concrete brittleness existed, i.e. the ductility was larger for smaller specimens. Next, three cyclic tests were performed on cubic concrete specimens during which the fatigue test parameters were as follows: the maximum stress σ_{max}=38.5 MPa and minimum stress σ_{min}=19 MPa with the stress level $S_{\max} = \sigma_{max}/f_c = 0.75$ and $S_{\min} = \sigma_{min}/f_c = 0.37$, and stress ratio $R = \sigma_{min}/\sigma_{max}$=0.5. The frequency of cyclic loading tests with the constant amplitude was always f=2 Hz. The assumed value of S was rational from the point of the design of concrete members in order to avoid the frequency effect. The frequency variations between 1 and 15 Hz have, namely, an insignificant effect on the fatigue strength provided that the maximum stress level is smaller than 75% of the monotonic static strength ([16, 17]). The expected fatigue life of concrete specimens was about N=60,000 cycles according to Model Code 2010 [14] ($\log N = (12 + 16S_{\min} + 8S_{\min}^2)(1 - S_{\max})$). Although the number of concrete specimens was low (3), the calculated fatigue experimental results were similar with respect to the number of loading cycles leading specimens to the failure, changes of cracks' and pores' volumes and cracks' distributions.

Experimental set-up

The cracking evolution in concrete during fatigue cyclic tests was investigated using the advanced X-ray micro-computed tomography system SkyScan 1173 (Figure 3). This system represents the newest generation in high-resolution desktop X-ray micro-tomography technologies for 3D scanning [20]. The technology defines the density of each specimen voxel by assigning different shades of grey (light grey shades correspond to high densities and dark grey shades correspond to low densities). The system was equipped with the high energy table open scanner with the 130 keV micro-focus X-ray source, flat panel sensor of the large format (5 Mpx) and special protection by a lead-glass fiber-optic window (Figure 3). The scanner possessed a precision object manipulator that allowed for a very precise and automatic specimen positioning. There were several filters available in the front of the X-ray detector: 0.25 mm brass filter, 1.0 mm aluminium filter, 2.0 mm lead filter and 0.25 mm copper filter. As compared to usual micro-tomography systems, it has two important advantages: a) large specimens up to 200 mm in diameter may be scanned and b) the specimens may be scanned with the high precision of 2-3 microns. During tests on concrete cubes, the X-ray source voltage was set on 130 keV, current on 61 μA and exposure time on 4000 ms. The pixel size was 34.2 μm. The X-ray projections were recorded with the rotation increment of 0.2° within 360°. To reduce the noise in X-ray projections, the frame averaging option was chosen to be 6 and the random movement option 10. The scanning time was equal to 6 hours. All specimens were scanned using the same input parameters. In order to recognize pores and cracks on micro-CT scans, a threshold procedure was carefully performed,

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based on the density of each concrete phase. The threshold in the range 0-60 from the grey level histogram 0-255 was chosen. The image reconstruction was carried out with the NRecon software. After the reconstruction, the images were analyzed with the CTAn software and finally the CTVox software was used to prepare the volume-rendering image reconstruction. The software programs were developed by the firm Bruker mico-CT (https://www.bruker.com/products/microtomography.html).

Figure 4 presents the view on three cubic specimens 40×40×40 mm^3 (called the specimens '1'-'3') before fatigue tests, based on the 3D micro-CT images. The micro-CT technology clearly reveals a heterogeneous 3D material meso-structure where aggregate, cement matrix, and pores are distinguishable on the images of specimens. The porous interfacial transitional zones (ITZs) around aggregate grains that are a very important concrete phase in inducing micro-cracks and attracting macro-cracks [26, 27] are not visible in scans due to their very small dimensions. However, they may be observed and measured on the concrete surface e.g. with the aid of the 2D scanning electron microscope (SEM) ([22-24]). The width of FPZs may be determined on the concrete surface by means of the digital image correlation (DIC) technique ([22-24]).

Distribution of pores

Figure 5 and Table 2 show the initial 3D distribution and content of pores in non-cracked concrete specimens '1'-'3' (intended for fatigue tests) of Figure 4 and '0' (intended for monotonic test). The pores were divided into the so-called closed and open ones. The open pores were defined as the pores that spread beyond the borders of the investigated specimen and the closed pores were defined as those in the specimen's interior. The initial pore volume in the specimens '1'-'3' was 1568.4 mm^3, i.e. 2.45% of the specimen volume (closed pores - 1.60% and open pores - 0.85%, Figures 4a and 5a), 1760.2 mm^3, i.e. 2.75% of the specimen volume (closed pores - 2.07% and open pores - 0.68%, Figures 4b and 5b) and 1516.8 mm^3, i.e. 2.37% of the specimen volume (closed pores - 1.98% and open pores - 0.39, Figures 4c and 5c). The pores with the diameter smaller than 1.0 mm constituted about 25-30%, the pores with the diameter 1.0 mm - 2.0 mm represented about 20-30% and the pores with the diameter larger than 2.0 mm formed about 40-50% of the total pore volume in concrete specimens. The specimen '0' that was subjected to monotonic static compression had the similar initial pore volume (1817.6 mm^3) as the specimens '1'-'3'.

3. Experimental results of fatigue compressive tests

The fatigue cyclic loading tests were carried out on 3 concrete specimens 40×40×40 mm^3 with the control of both the stress level and stress ratio. The continuous fatigue tests were performed for the

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specimens ‘1’ and ‘2’. For those specimens, the initial (non-cracked specimens) and final (cracked specimens) micro-CT images were only shot whereas for the specimen ‘3’, some micro-CT scans were shot during the entire fatigue test. The specimens were always unloaded for scanning (scanning lasted each time 6 hours). Next, the compression test was continued. The scanning took place after N_i=10,000, 30,000, 60,000 and 70,000 cycles, so in total, five 3D micro-CT scanning series were performed (including initial scans before the tests). Note that unloaded periods for scanning may slightly affect fracture since some crack recovery (cracks’ closure) occurred during those rest periods [38]. The number of loading cycles leading specimens to the failure (fatigue life cycles) of the specimens ‘1’-‘3’ is shown in Table 3. It was between N=71,000 and 80,000 cycles (i.e. slightly higher than that (60,000) according to [14]).

The stress-displacement diagrams σ=f(u) for the concrete specimens ‘1’-‘3’ during the cyclic fatigue tests as compared to the monotonic static test is shown in Figure 6. Figure 7 presents the zoom on the experimental vertical displacement u of the specimen ‘3’ in cyclic uniaxial compression versus the cycle number N_i with the marked breaks for scanning. In the monotonic test, the curve σ=f(u) included obviously the elastic, hardening and softening region (Figure 6).

The external 3D micro-CT images of cubic cracked concrete specimens ‘1’-‘3’ and ‘0’ are presented in Figure 8. The specimens ‘1’-‘3’ were scanned close to failure (Table 3) for N_i=70,000 and the observed pattern of pores including cracks is shown in Figure 9. Table 4 includes the volumes of pores and cracks in concrete specimens ‘1’-‘3’ after 70,000 cycles and in the specimen ‘0” after the monotonic test.

After the tests, the specimens were strongly cracked (Figures 8 and 9). The vertical cracks that propagated through the entire specimen height were predominant. There existed 6, 2 and 4 main vertical macro-cracks in the entire concrete specimens ‘1’-‘3’ (Figure 8). Moreover, in the specimens ‘1’ and ‘3’ some diagonal cracks can also be observed. The cracking slightly varied along the height of specimens due to the effect of boundary conditions in tests [39, 40]. The cracks were curved due to the presence of stochastically located aggregate particles. Initially, the cracking process was induced due to some stress concentrations close to the cube corners (see Figures 12 and 13) where the inclined micro-cracks appeared and coalesced. Next, some vertical cracks started to concentrate along lateral both edges and surfaces of specimens by forming column-like regions. The macro-cracks were the widest on external parts of concrete cubes at lateral edges that finally lead to concrete spalling from specimen cores [23], [41]. The concentration extent of cracking regions throughout the specimen was similar in monotonic and fatigue tests, based on the visual inspection (compare Figures 9b and 9d). However, wider macro-

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cracks (compare Figures 9a and 9c) and more damaged aggregate particles were noticed during fatigue tests.

Due to cracking, the insignificant volumetric changes of open and the pronounced changes of closed pores happened during fatigue tests (Table 4, Figure 10). The crack volume was calculated as the total volume of pores in the cracked specimen reduced by the total volume of pores in the initial non-cracked specimen. The cracks' volume and the %-volume of open pores increased in all specimens. In contrast, the %-volume of closed pores decreased in the specimens The cracks' volume increased during fatigue test by 3.43%-5.62% in the specimens '1'-'3'. The %-volume of open pores increased by 1.86%-4.38% and the %-volume of closed pores decreased by 0.2%-0.74%. The increase of the cracks' volume and open pores in the specimen '0' (monotonic test) was smaller on average by about 30% than during fatigue tests. The greatest macro-crack width in the entire specimens' volume (after unloading) was w_c=0.42 mm (specimen '0'), w_c=0.61 mm (specimen '1'), w_c=0.56 mm (specimen '2') and w_c=0.72 mm (specimen '3'). The pores were practically not crossed by cracks since insignificant volume changes of closed pores took place (connected with strong volume changes of open pores) (Table 4).

Figure 11 shows the cross-sectional micro-CT images of the cracked specimens '1'-'3' and '0' (one horizontal and two vertical in the mid-specimen that intersected the specimen centroid). They show that cracks mainly propagated through the cement matrix and ITZs which were the weakest zones in concrete. The micro-cracks occurred first in porous ITZs around aggregate particles and then they connected themselves through a bridging mechanism ([22-24]). When two interfacial cracks happened around adjacent aggregate particles, a crack inside the cement matrix bridged those interfacial cracks so that a connected crack path was formed. The cracks also propagated sometimes through single weak aggregate particles (Figure 12). The cracks' branching also occurred (Figure 12).

Figures 13 and 14 show the external 3D micro-CT images of the concrete specimen '3'for the different cycle number N_i: N_1=0 (step "0" - initial scan), N_3=30,000 (step "2"), N_4=60,000 (step "3") and N_5=70,000 (step "4"). The results for N_2=10,000 were not presented since the cracks insignificantly developed. The different three cross-sectional micro-CT images of the mid-region (one horizontal and two vertical that intersected the specimen centroid) for the different number of loading cycles N_i are demonstrated in Figure 15.

For N_i=10,000 cycles (Figure 15B), the thin cracks occurred with the width up to w_c=0.04 mm. The cracks had an irregular shape and were mainly concentrated along one vertical (lateral) edge of the specimen. All micro-cracks occurred in ITZs between the cement matrix and aggregate particles and

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propagated next in the cement matrix. For N_3=30,000 cycles (Figures 13b, 14b and 15C) further development of existing internal cracks took place (they propagated into the depth of the cement matrix) and the new macro-cracks occurred (one at the other lateral edge and one on the lateral surface). In total, 7 broken aggregate particles were detected in the entire specimen. The greatest crack width in the entire volume was w_c=0.16 mm. After N_4=60,000 cycles (Figures 13c, 14c and 15D) the existing vertical macro-cracks further evolved along lateral edges and two of those cracks propagated through the specimen height. The maximum crack width was w_c=0.42 mm. The number of broken aggregate particles was 13. For N_5=70,000 cycles (Figures 13d, 14d and 15E), four main vertical macro-cracks of an irregular shape and a variable width might be observed (two cracks were located along two lateral edges and two cracks were concentrated on the lateral surface of the specimen). The macro-cracks intersected the concrete specimen. In addition, one macro-crack occurred along a horizontal edge and one inclined macro-crack appeared in the upper region on the second lateral surface. The main macro-cracks were connected through a network of small cracks. The largest crack width was equal to w_c=0.72 mm. The number of broken aggregate particles increased up to 28. Finally, the specimen damage occurred along the edge wherein the dominant vertical macro-crack was located.

Table 5 and Figures 16 and 17 present the detailed data on the volume changes of pores and cracks in the concrete specimen '3' with increasing damage parameter (expressed by the quotient of the number of cycles N_i and the fatigue life N=73,127, Table 3). The line connecting the measurement points was approximated in Figures 16 and 17 by a polynomial function. The volume of closed pores slightly decreased during the entire test (Figure 16). In the step "1", the insignificant volume changes of open pores and cracks were obtained as compared to the step '0'. The maximum crack width in the entire volume was w_c=0.04 mm (after the specimen unloading). In the step "2", the volume of pores and cracks increased by about 50%. The greatest crack width in the entire volume was w_c=0.16 mm (after the specimen unloading). In the step "3", the volume of pores and cracks increased as compared to the step '2' by about 40%. The maximum crack width in the entire volume was w_c=0.42 mm (after the specimen unloading). In the last step "4", the volume of pores and cracks increased as compared to the step '3' by about 40%. The largest crack width in the entire volume was w_c=0.72 mm. (after the specimen unloading). The increase of the cracks' volume with increasing damage parameter was strongly non-linear. The relationship in Figure 17 may be divided into three parts: 1) between the damage parameter 0 (N_1=0) and damage parameter 0.14 (N_2=10,000) (so-called the micro-crack part), 2) between the damage parameter 0.14 (N_2=10,000) and damage parameter 0.85 (N_4=60,000) (so-called the transitory part) and 3) between the damage parameter 0.85 (N_4=60,000) and damage parameter ~1.0 (N_5=70,000) (so-called the crack extension part [41]) (Figure 17). The damage rate was in particular strong in the last fatigue stage (crack extension region) between N_4=60,000 and N_5=70,000 cycles.

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In Figures 18 and 19, the attention is focused on the largest crack volume growth in the crack extension region before the specimen failure. The volume of cracks between those 2 different cycles' numbers increased by 2.26% (40% of the total cracks' growth) (Figure 18d, Table 5). The %-volume of closed pores decreased from 1.34% down to 1.24% (the decrease of about 10%) and the %-volume of open pores increased from 4.39% up to 6.75% (the increase of about 50%). The width of cracks, which was very non-uniformly distributed in the specimen, increased on average by 0.1-0.2 mm (Figure 18). However, in some specimen regions, it increased even by 0.3 mm.

Our experiments on concrete fatigue will be continued. An extended X-ray micro-computed tomography system will be used soon, i.e. the tomography system SkyScan 1173 will be connected to the loading machine ISTRON 5569 to make images of deforming concrete specimens during a continuous deformation process, i.e. without unloading for scanning.

4. Conclusions

This paper presents the results of experimental research work showing the 3D fracture evolution in plain concrete specimens under fatigue compression obtained by X-ray micro-CT that is a powerful tool to measure the internal damage of concrete specimens. For plain concrete under fatigue compression, the following conclusions can be offered:

- The increase of the cracks' volume with increasing damage (expressed by the quotient of the number of cycles and fatigue life) was about hyperbolical in shape. The volume of cracks close to the failure load was 3.4-5.6% of the entire specimen volume during fatigue tests. Due to cracking, the %-volume of closed pores decreased by about 30% and the %-volume of open pores increased 5-15 times. In the last loading stage between 60,000 and 70,000 cycles, the cracks' volume strongly increased (by 2.26%), i.e. almost 40% of the total crack volumetric growth.

- The growth of the total fracture volume in fatigue tests was higher by 30% as compared to the monotonic test.

- A similar crack pattern was obtained in specimens under monotonic and cyclic loading although the latter was on more damaged. The cracking pattern was strongly non-uniform. The greatest cracks' width was in the range of 0.56-0.72 mm (fatigue tests) and 0.42 mm (monotonic test). The cracks that initially occurred in ITZs and propagated through the cement matrix by bridging, were strongly curved. However,

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several cracks also propagated through weak aggregate particles. At the failure, the lateral sides of specimens separated from the cores.

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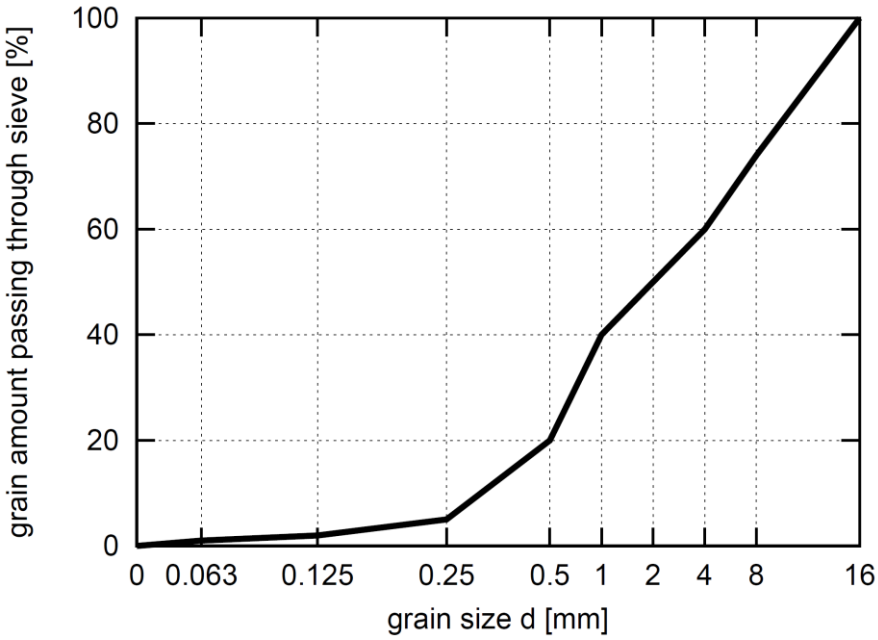

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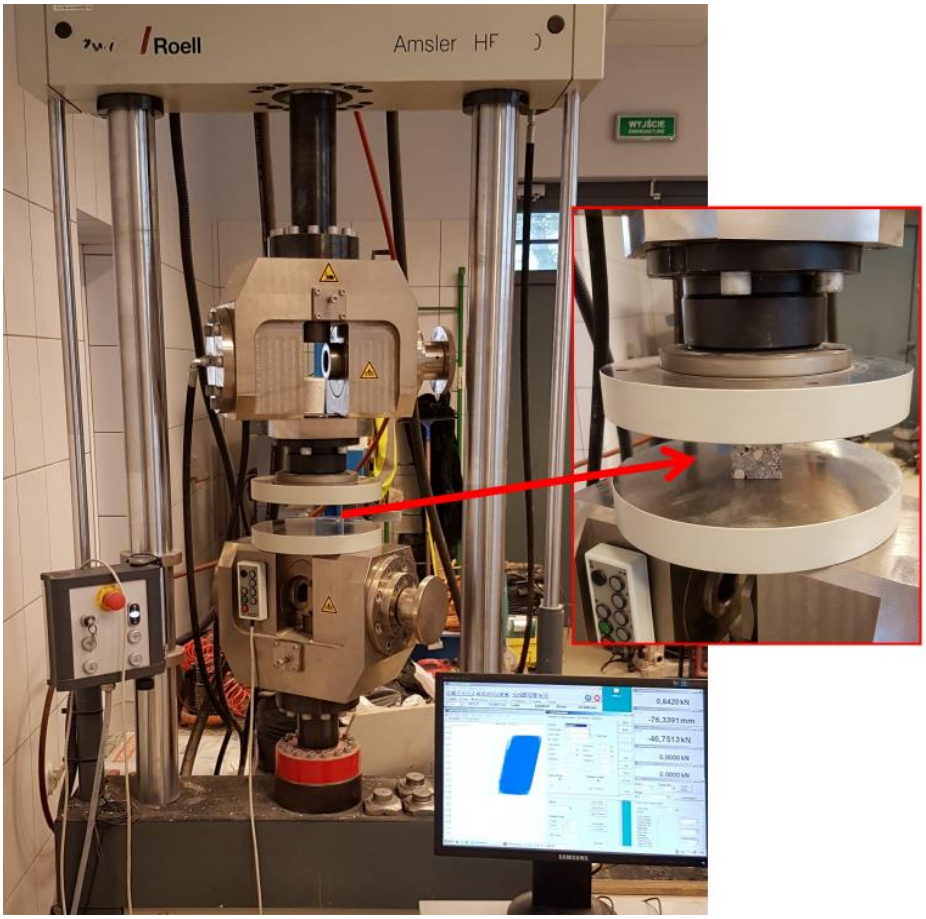

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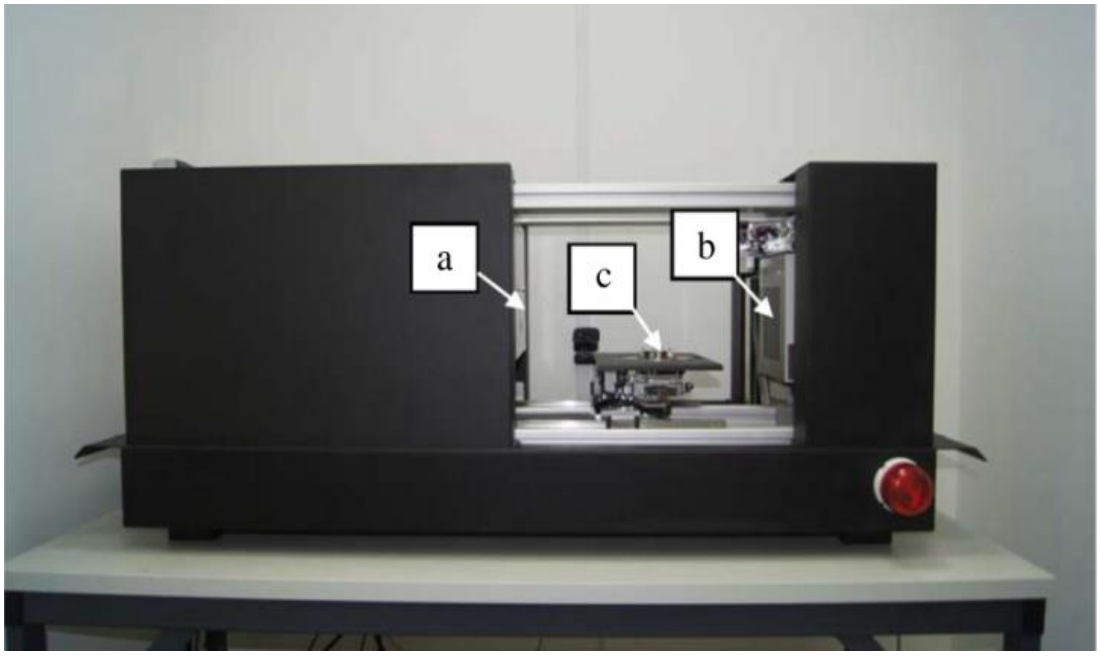

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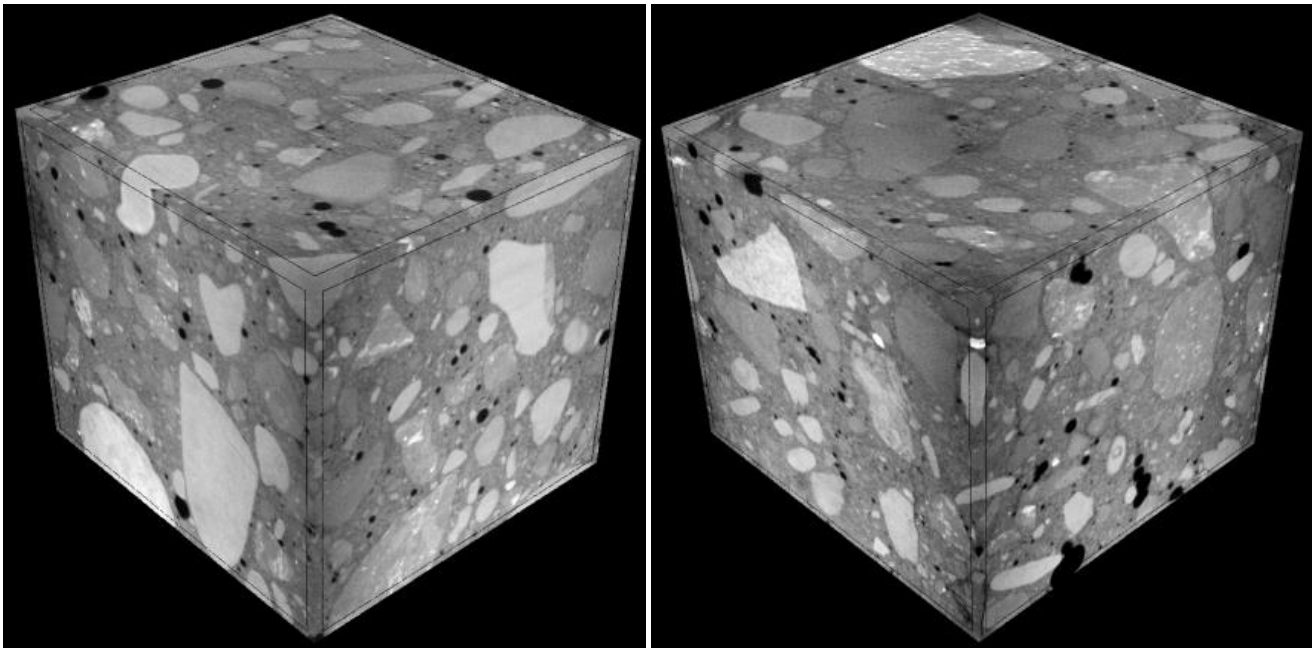
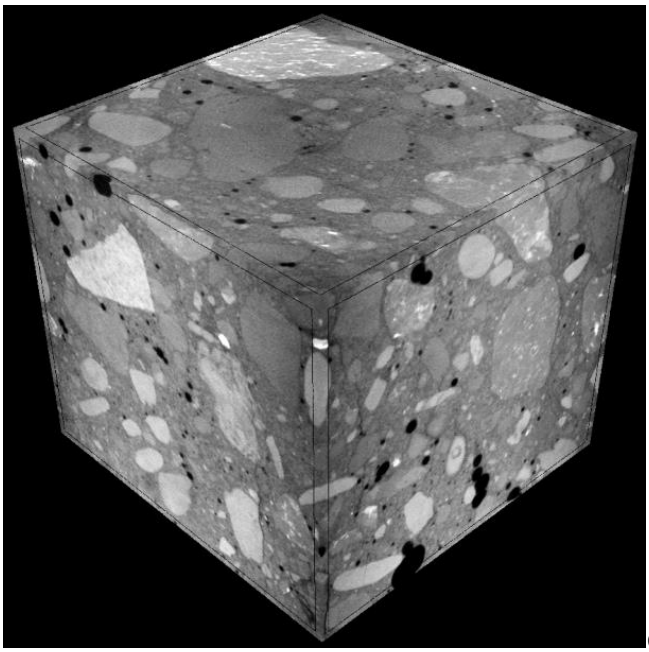


a) b)



c)

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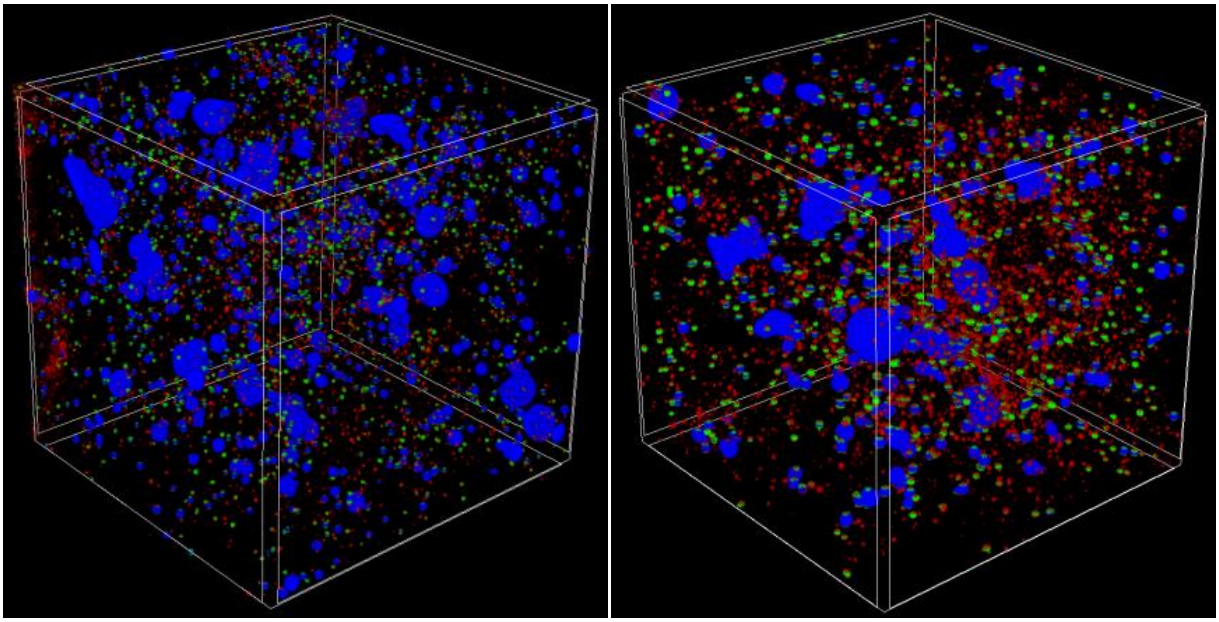
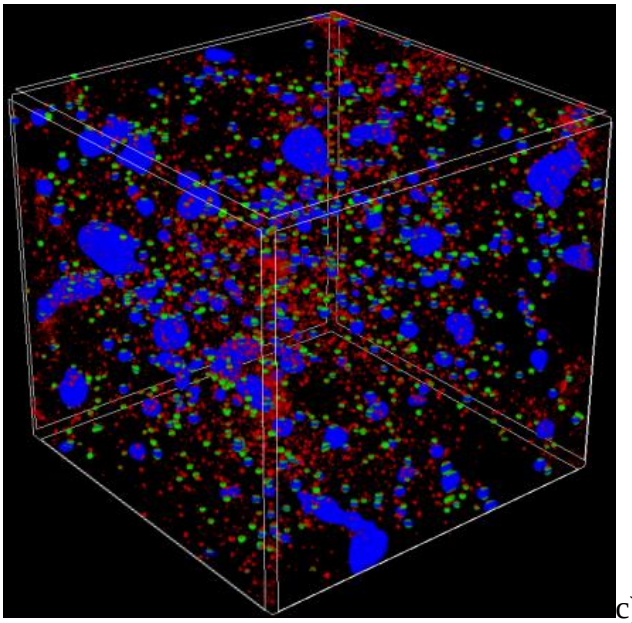


a) b)



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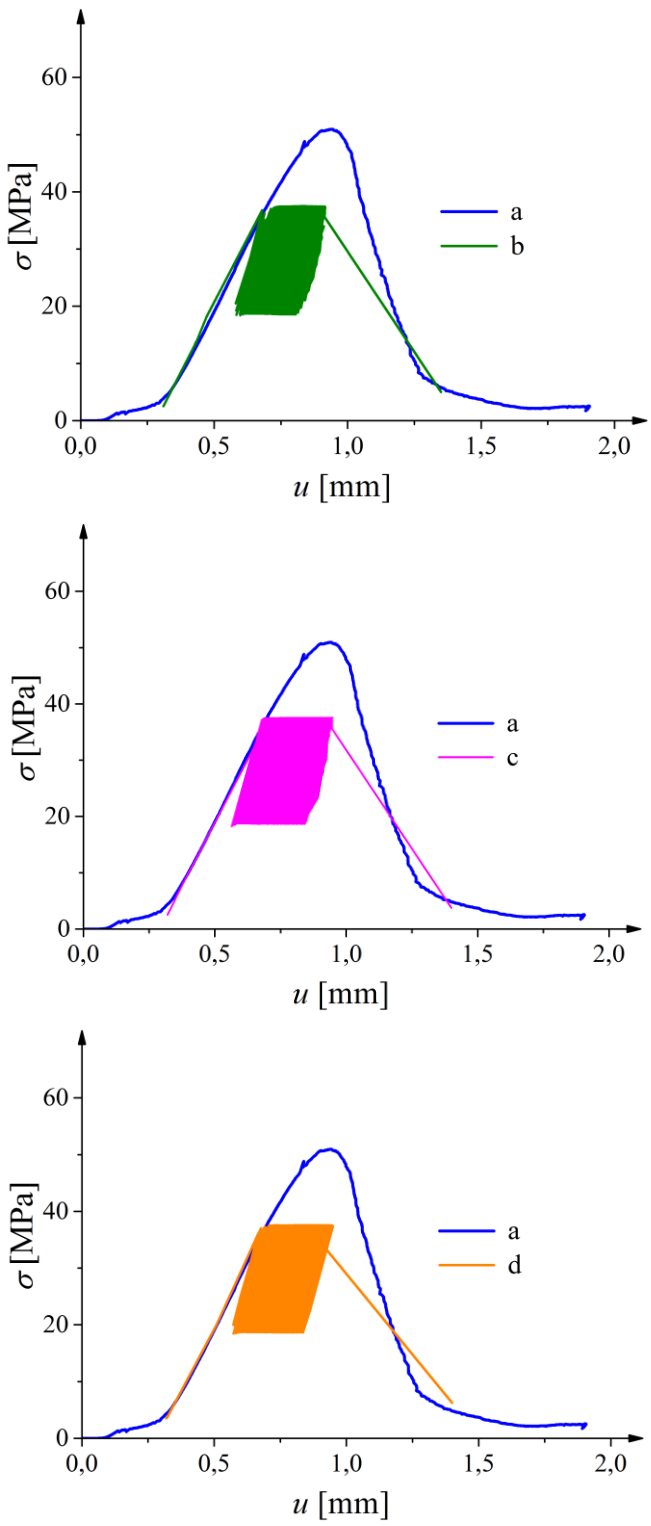

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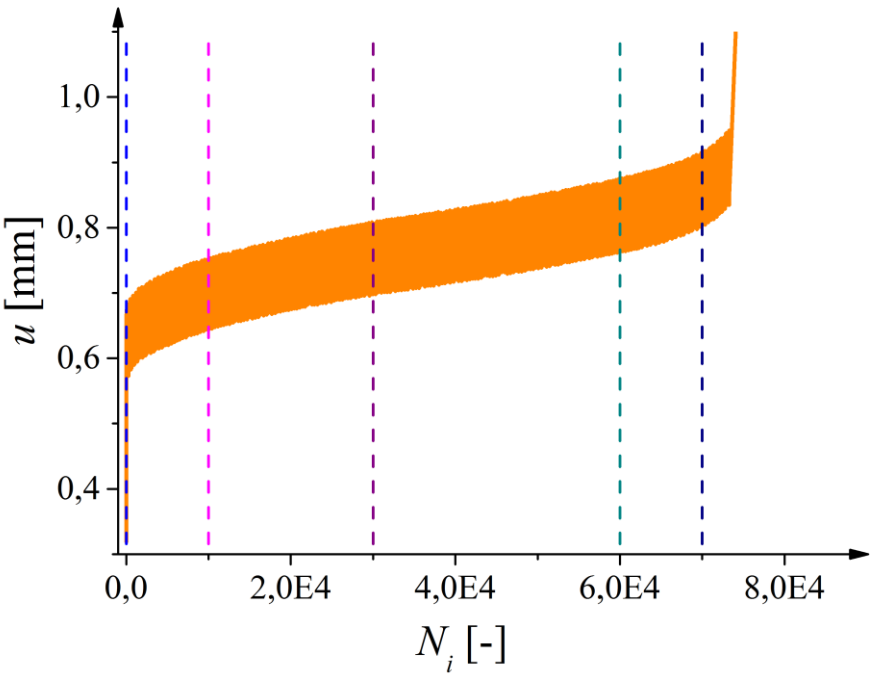

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FIGURE 7

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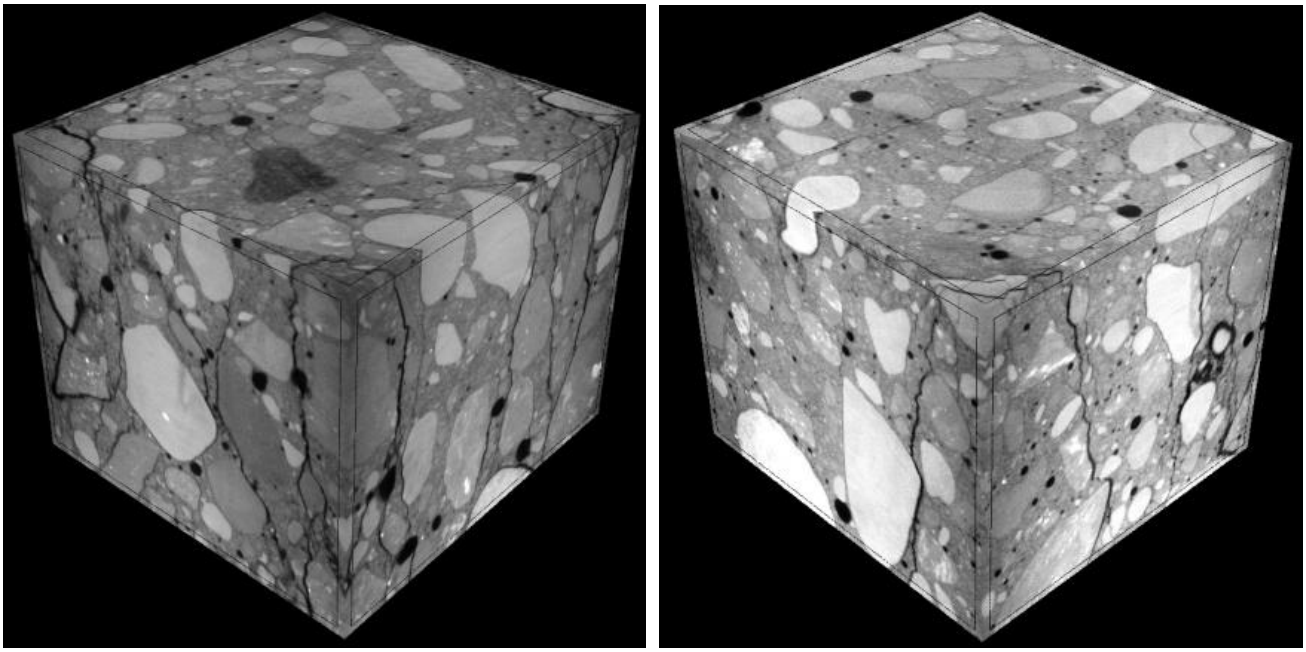

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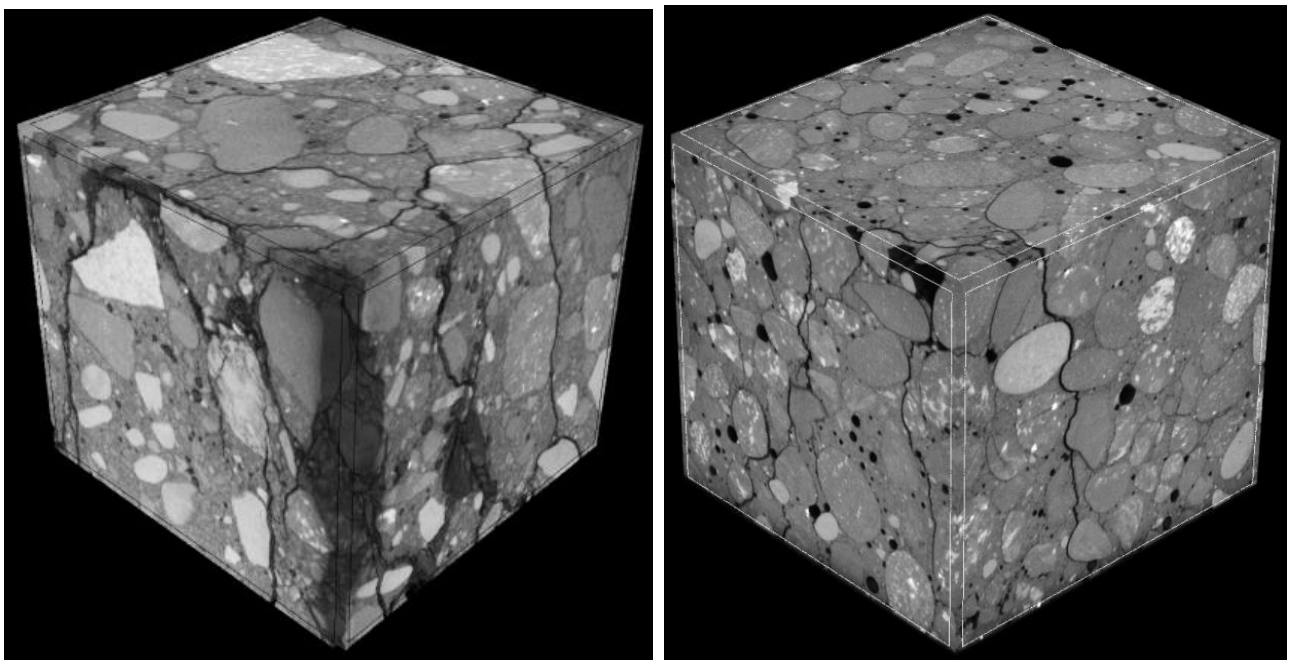

c) d)

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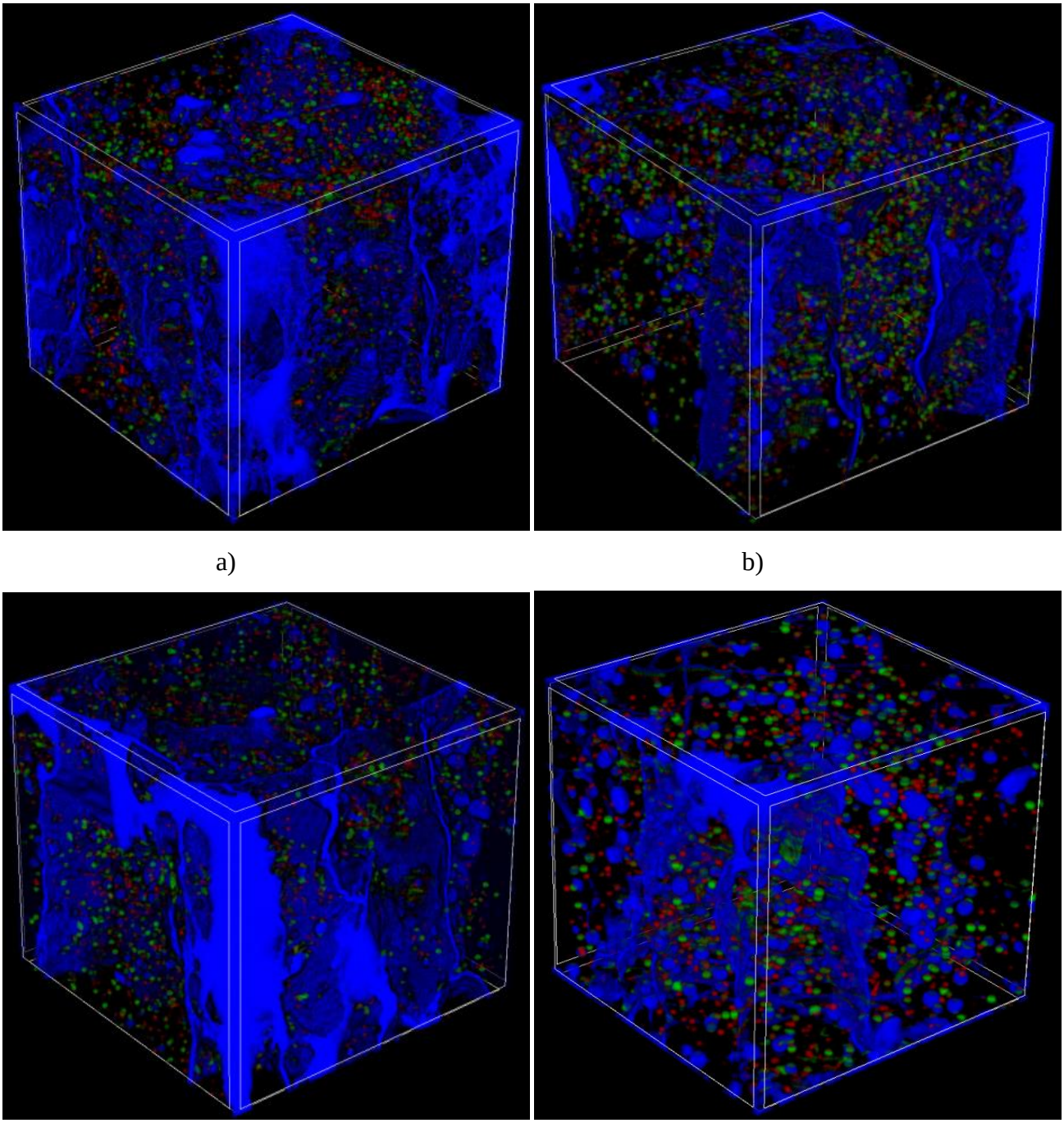

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FIGURE 9

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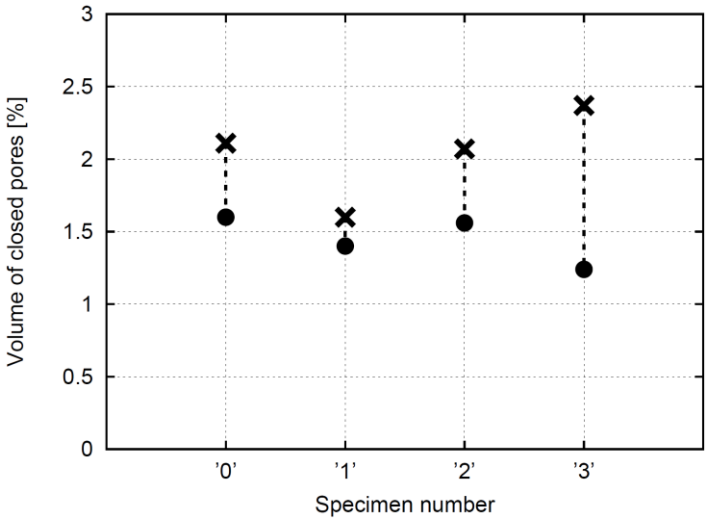

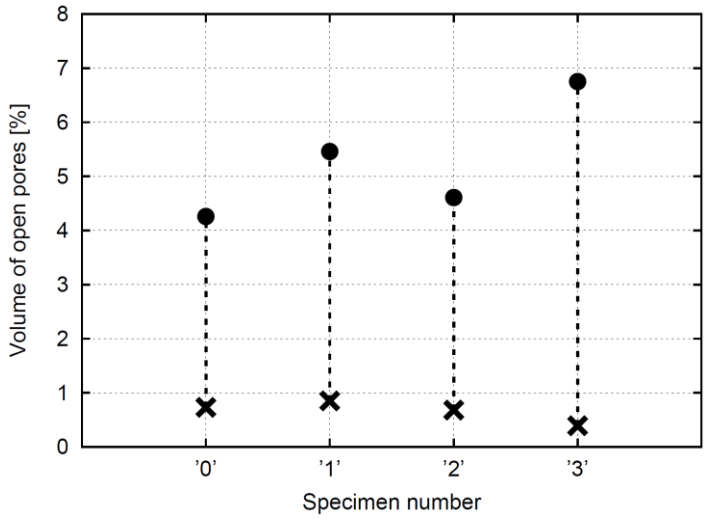

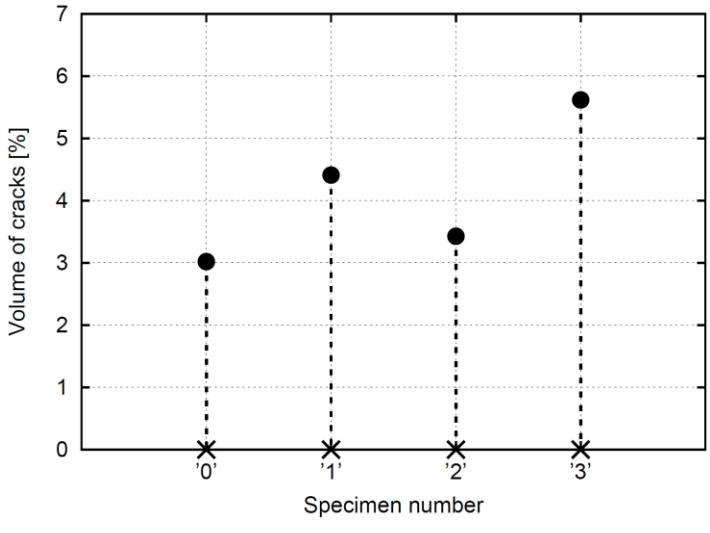

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FIGURE 10

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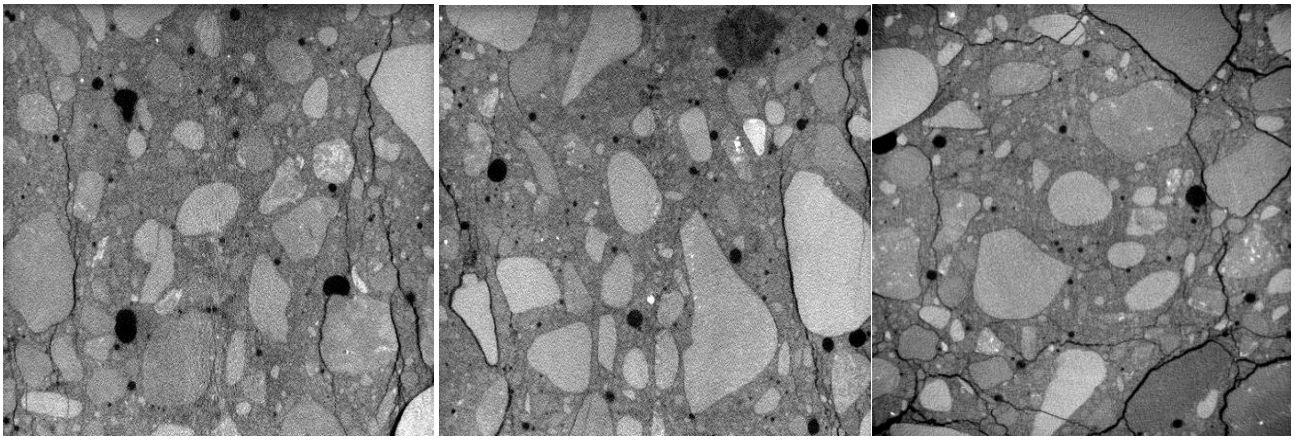

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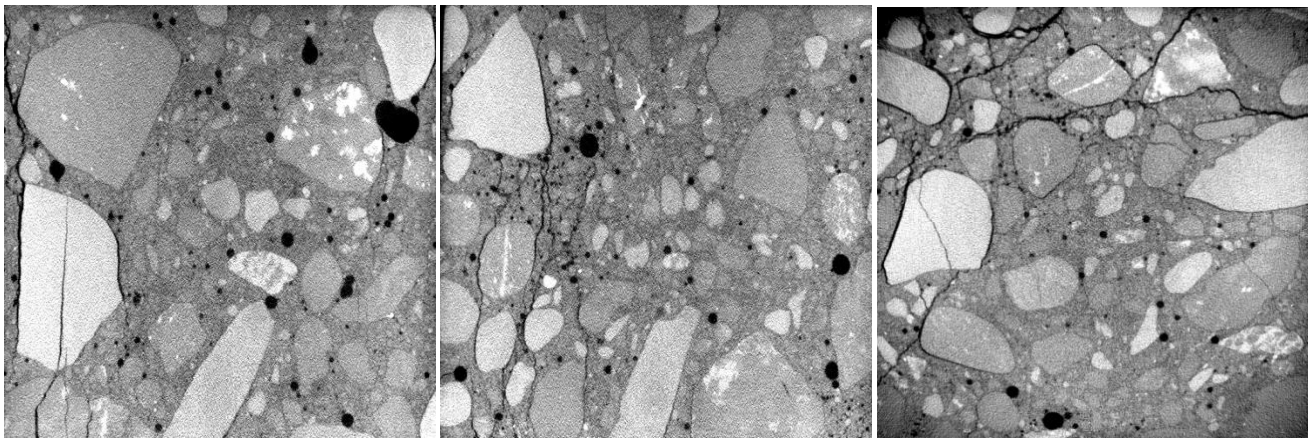

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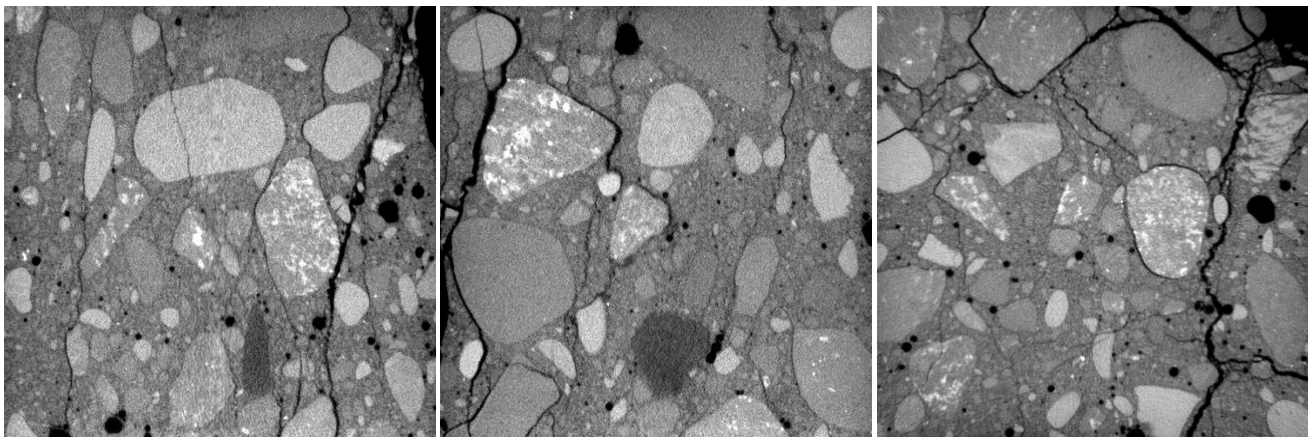

C)

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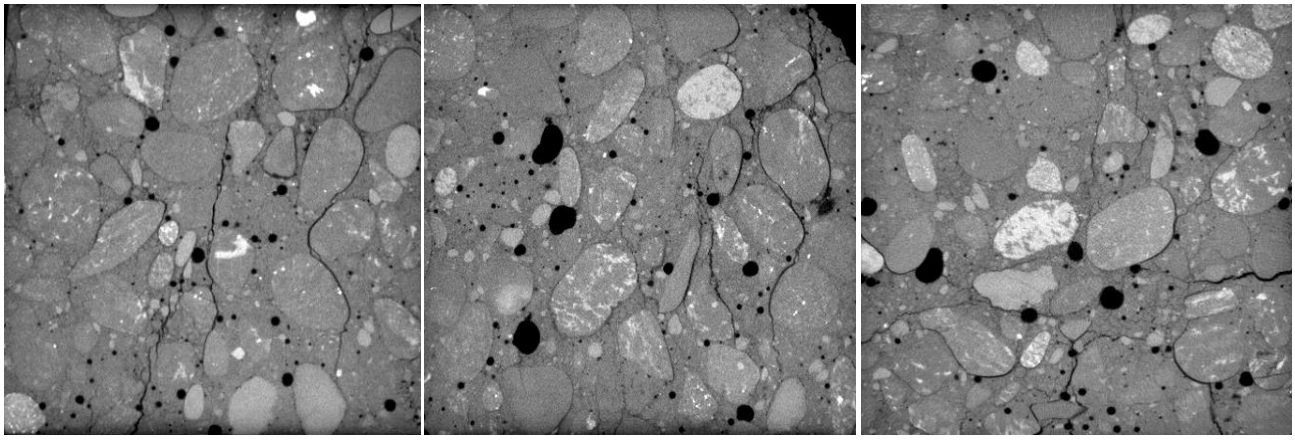

D)

a) b) c)

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FIGURE 11

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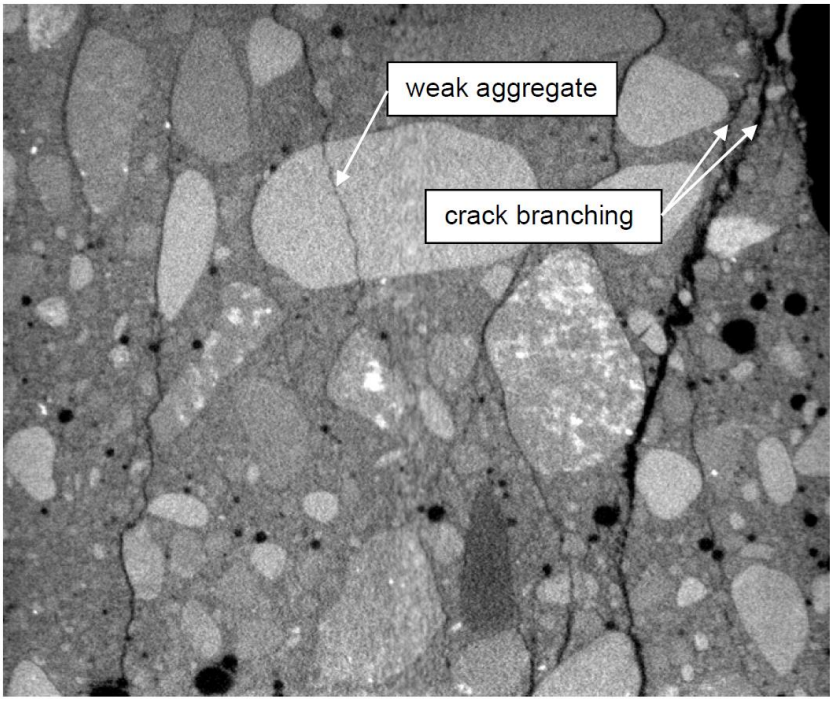

Figure 12: View on crack branching and crack propagating through weak aggregate particle

FIGURE 12

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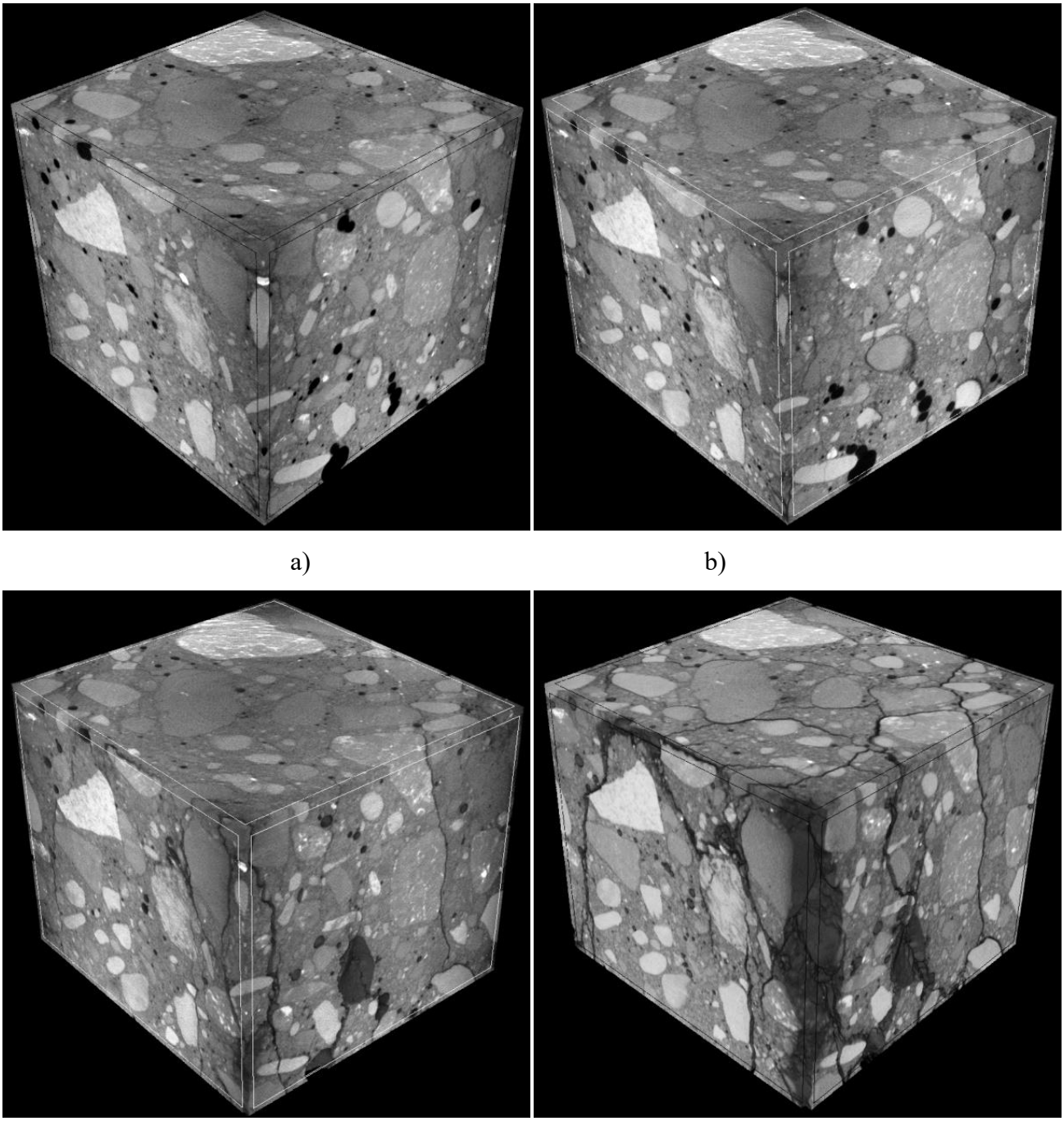

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FIGURE 13

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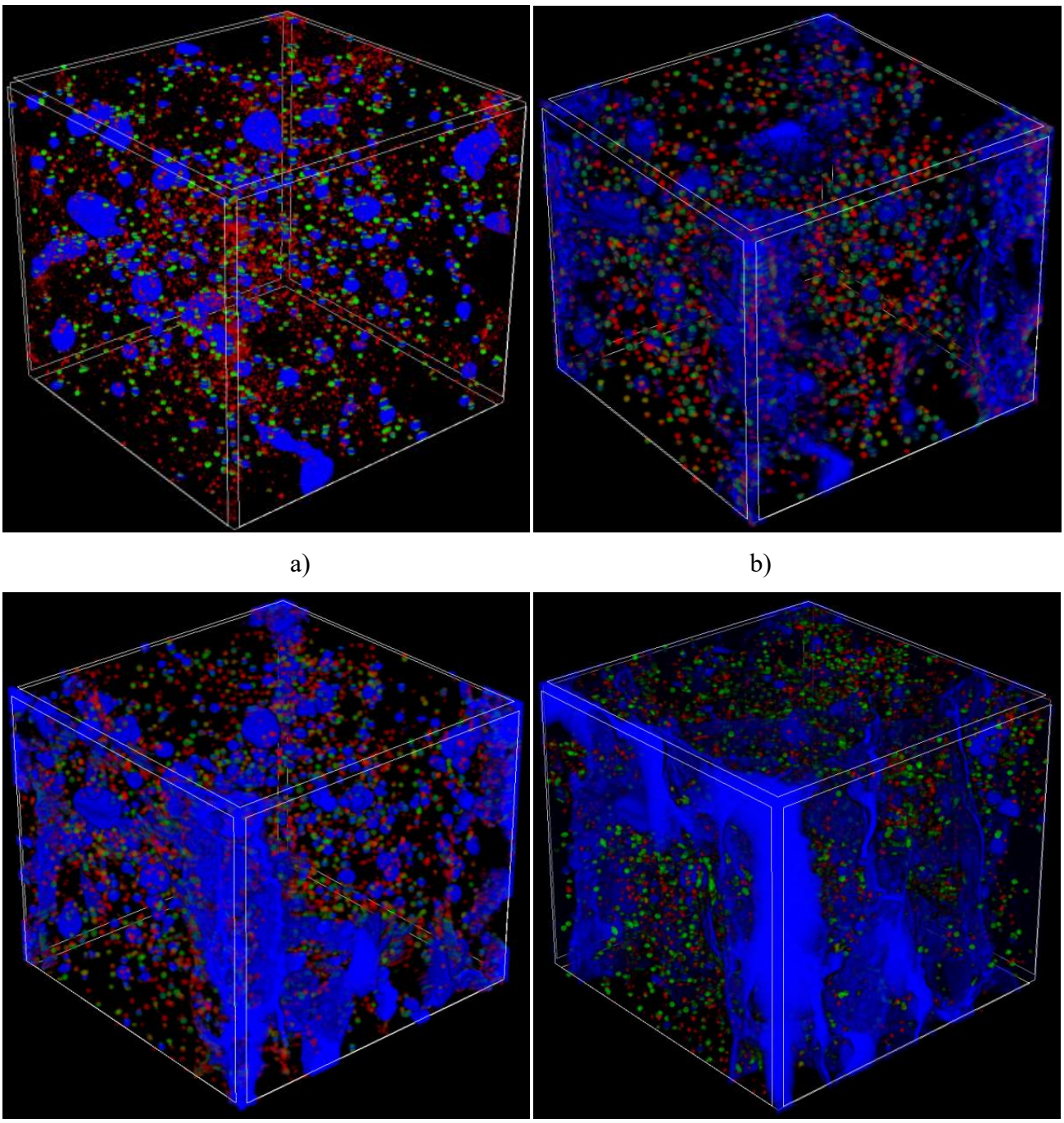

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FIGURE 14

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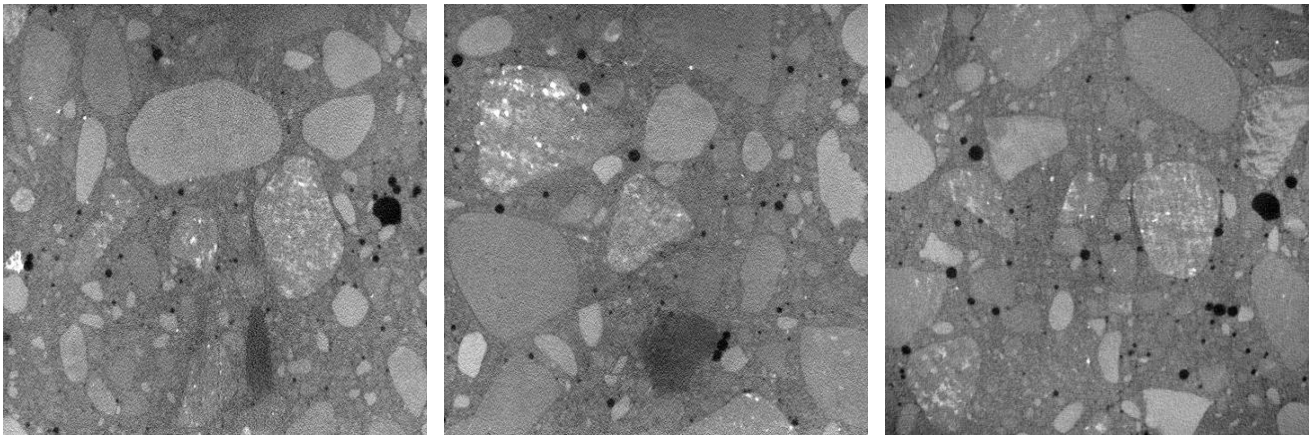

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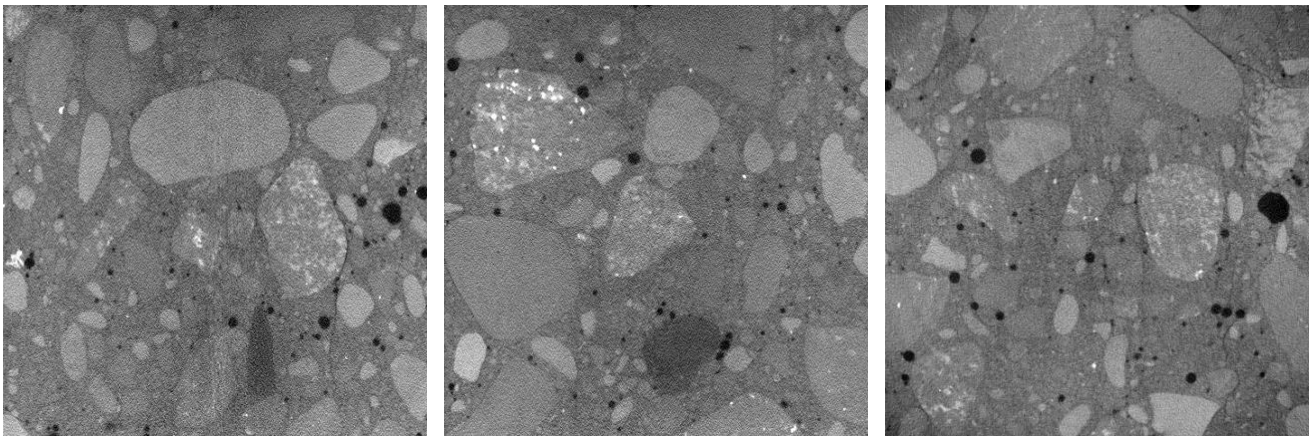

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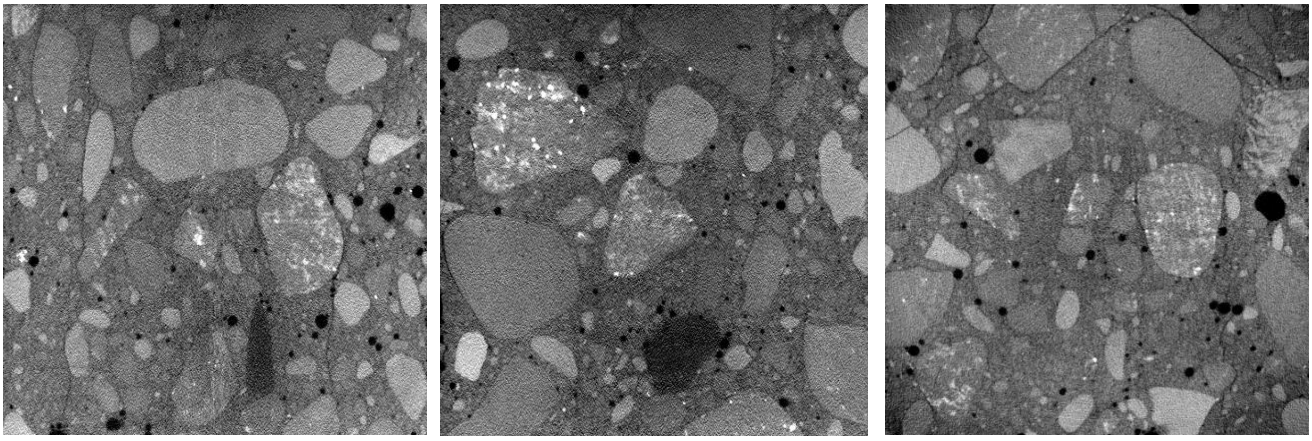

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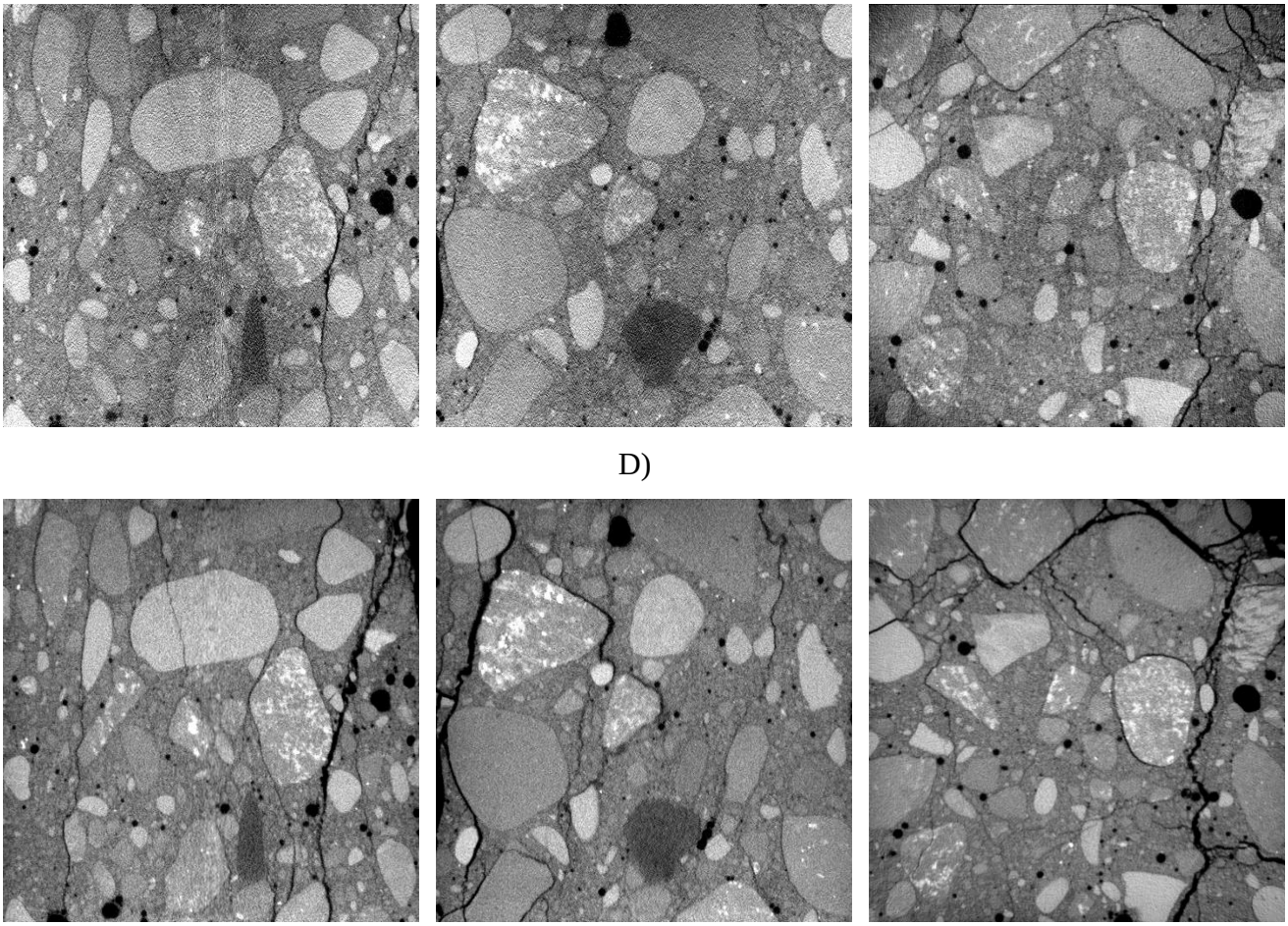

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FIGURE 15

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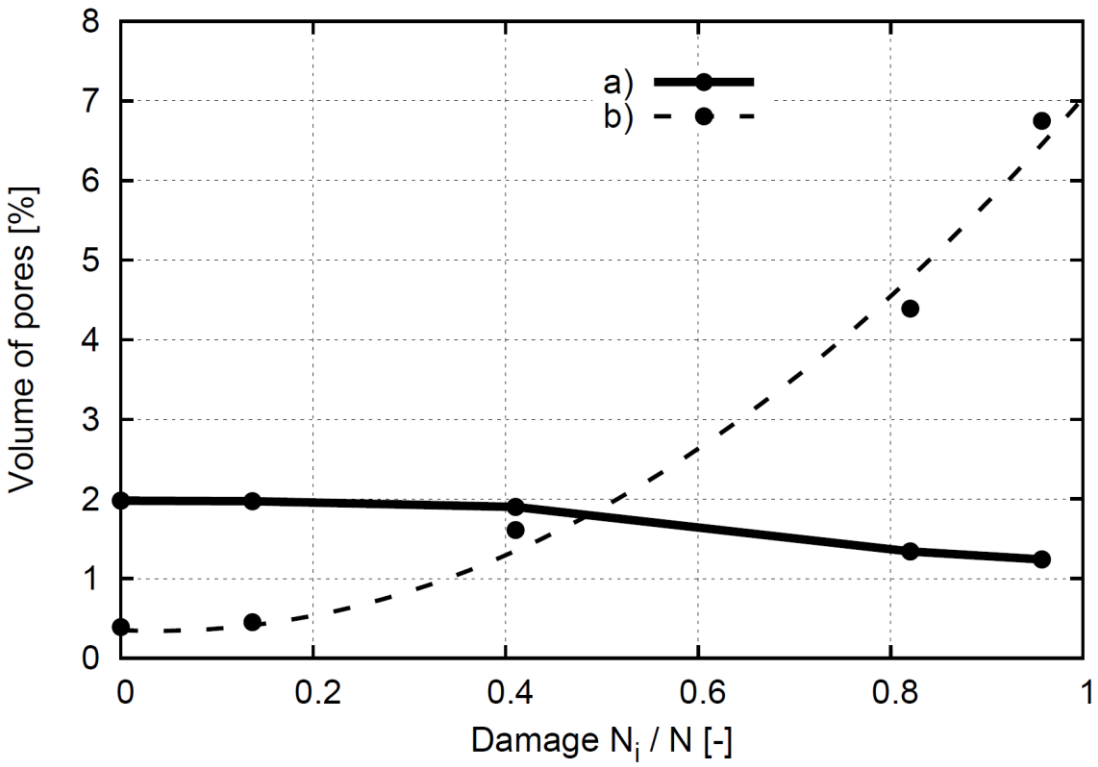

Figure 16: Evolution of volume of closed pores (a) and open pores (b) with increasing damage (expressed by quotient of number of loading cycles N_i and fatigue life N) in concrete specimen '3'

FIGURE 16

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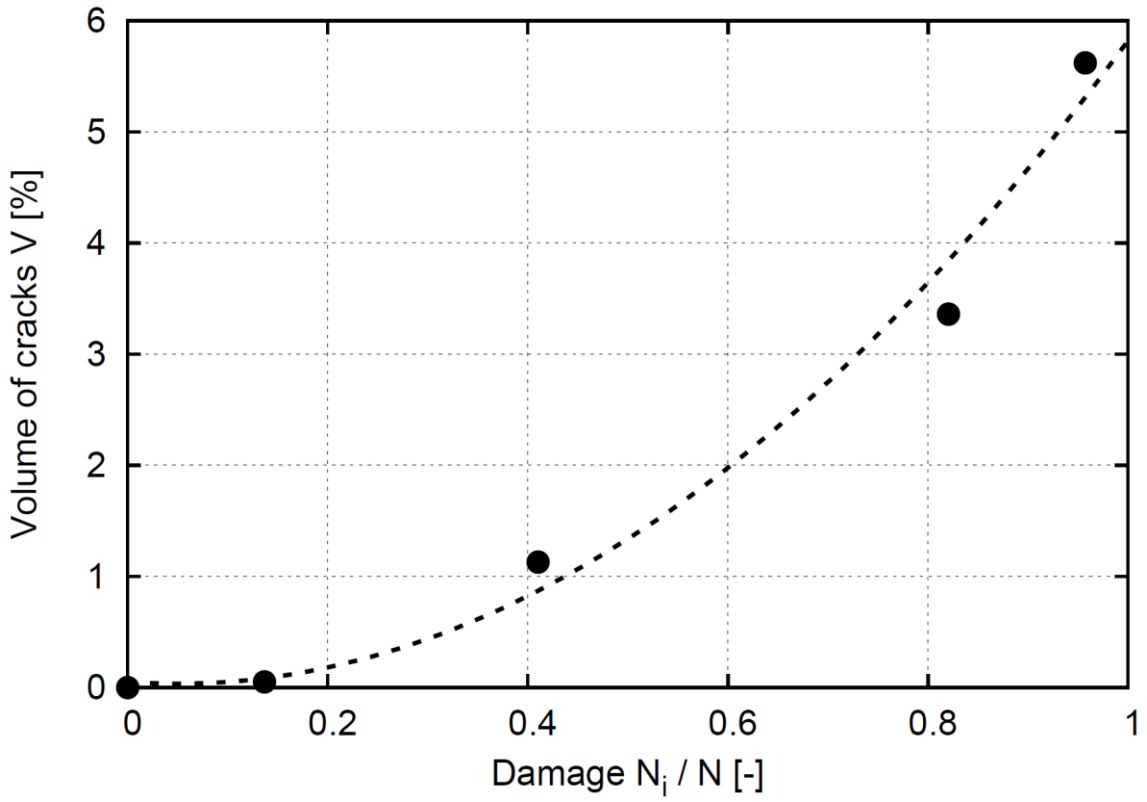

Figure 17: Evolution of crack volume *V* versus damage (expressed by quotient of number of loading cycles N_i and fatigue life *N*) in concrete specimen '3'

FIGURE 17

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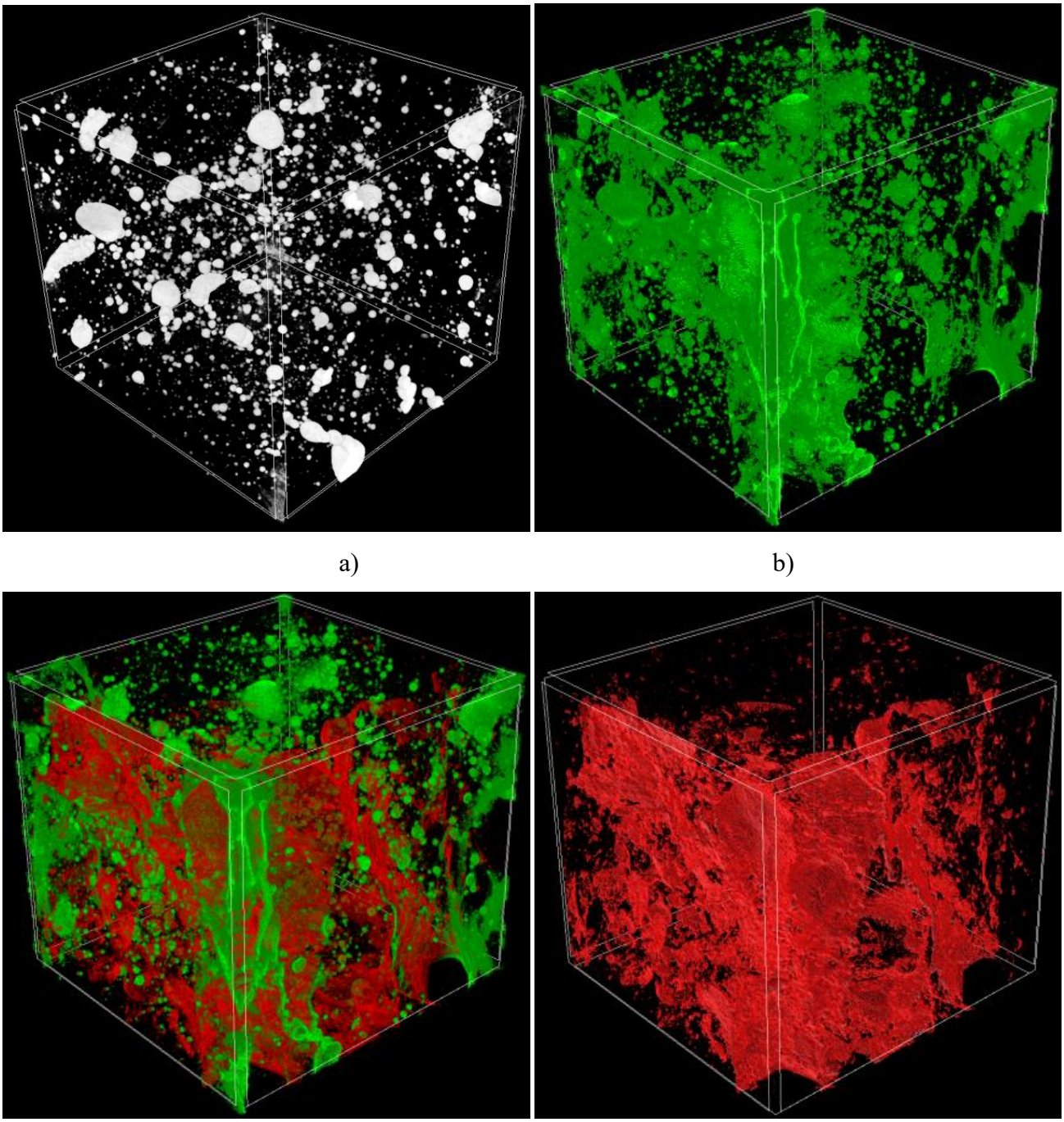

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FIGURE 18

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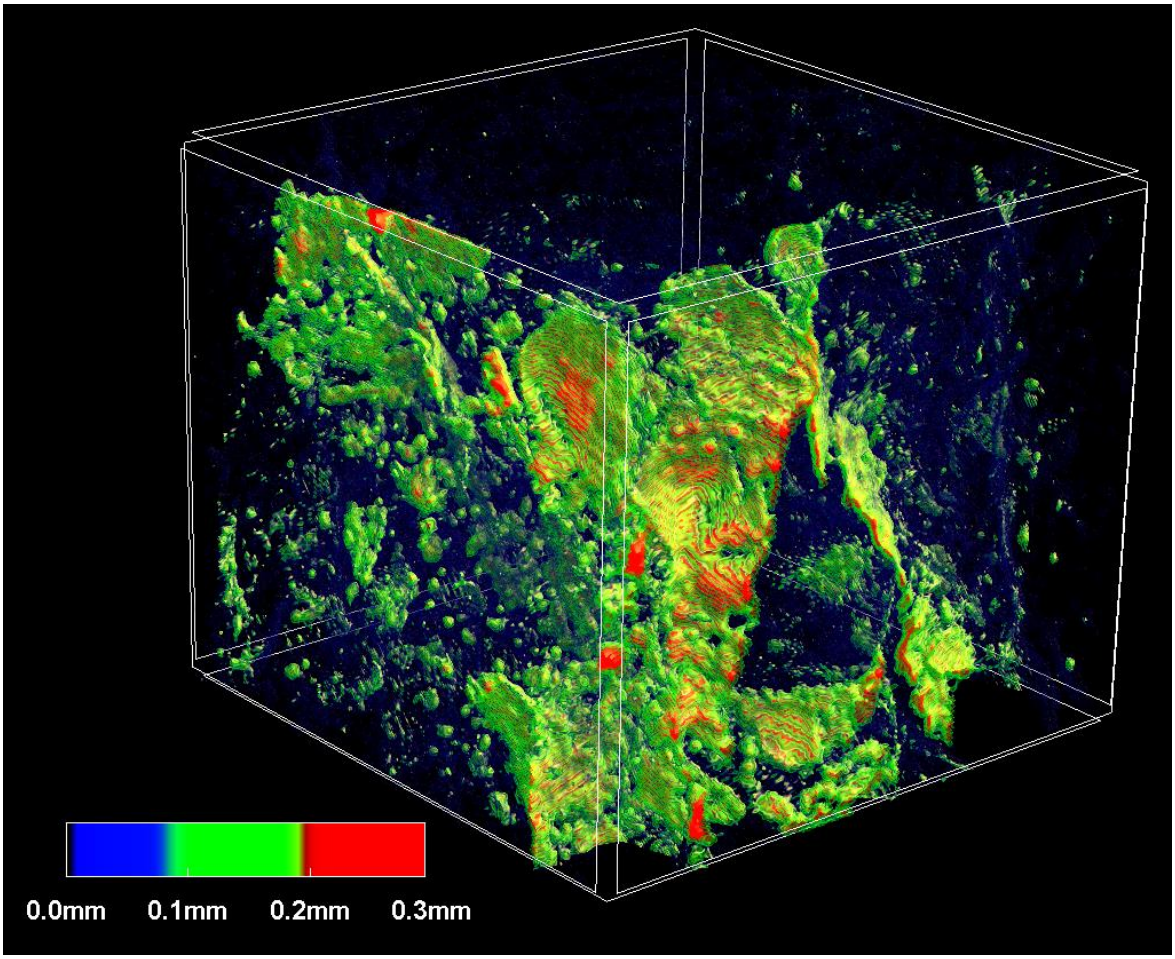

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FIGURE 19

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Table 1: Concrete mixing composition in experiments (d_{50} – mean particle diameter, d_{max} – maximum particle diameter and β – total particle volume)

Concrete component	**Content of concrete components** (d_{50}=2 mm, d_{max}=16 mm, β=75%)
cement (Portland 32.5R)	810 [kg/m^3]
sand (diameter size 0-2 mm)	650 [kg/m^3]
gravel (diameter size 2-8 mm)	580 [kg/m^3]
gravel (diameter size 8-16 mm)	580 [kg/m^3]
water	340 [l/m^3]

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Table 2: Volume and diameter range of macro-pores in initial non-cracked concrete specimens (specimens ‘1’-‘3’ are presented in Figure 4)

Specimen number and test type	Diameter range of pores [%]				Volume of pores [mm^3]	% - volume of pores [%]	% - volume of closed pores [%]	% - volume of open pores [%]
	≤0.50 mm	0.51-1.00 mm	1.01-2.00 mm	≥2.01 mm				
‘0” monotonic test	12.2	11.9	28.5	47.4	1817.6	2.84	2.11	0.73
‘1’ fatigue test	10.2	15.4	30.5	43.9	1568.4	2.45	1.60	0.85
‘2’ fatigue test	14.5	16.4	22.2	46.9	1760.2	2.75	2.07	0.68
‘3’ fatigue test	9.8	14.1	24.5	51.6	1516.8	2.37	1.98	0.39

Table 3: Fatigue life results (maximum number of loading cycles leading to specimen failure) for concrete specimens ‘1’-‘3’ during uniaxial compression (σ_{max} - maximum normal stress, σ_{min} - minimum normal stress and f_c - uniaxial compressive strength)

Concrete specimen	σ_{max}/f_c	σ_{min}/f_c	Number of fatigue life cycles
‘1’	0.75	0.37	71,518
‘2’			80,069
‘3’			73,127

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Table 4: Volume of pores and cracks in concrete specimens ‘1’-‘3’ after 70,000 cycles and in concrete specimen ‘0’ after monotonic loading close to failure

Specimen number and test type	Volume of pores and cracks [mm^3]	% - volume of pores and cracks [%]	% - volume of closed pores and cracks [%]	% - volume of open pores and cracks [%]	Volume of cracks [mm^3]	% - volume of cracks [%]
‘0’ monotonic test	3750.4	5.86	1.60	4.26	1932.8	3.02
‘1’ fatigue test	4390.4	6.86	1.40	5.46	2822.0	4.41
‘2’ fatigue test	3948.8	6.17	1.56	4.61	2188.6	3.43
‘3’ fatigue test	5113.6	7.99	1.24	6.75	3596.8	5.62

Table 5: Volume of pores and cracks in concrete specimen ‘3’ for different steps related to numbers of cycles N_i

Step	Number of cycles N_i	Volume of pores and cracks [mm^3]	% - volume of pores and cracks [%]	% - volume of closed pores and cracks [%]	% - volume of open pores [%]	Volume of cracks [mm^3]	% - volume of cracks [%]
‘1’	0	1516.8	2.37	1.98	0.39	0	0
‘2’	10,000	1548.8	2.42	1.97	0.45	32.0	0.05
‘3’	30,000	2240.0	3.50	1.90	1.61	723.2	1.13
‘4’	60,000	3667.2	5.73	1.34	4.39	2150.4	3.36
‘5’	70,000	5113.6	7.99	1.24	6.75	3596.8	5.62

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