

Piotr LEŚNIEWSKI, Kazimierz GOHRA

GDANSK UNIVERSITY OF TECHNOLOGY, FACULTY OF ELECTRICAL AND CONTROL ENGINEERING, HIGH VOLTAGE AND ELECTRICAL APPARATUS

Voltage dips reduction with a hybrid contactless short-circuit limiter

Mgr inż. Piotr LEŚNIEWSKI

He was born in 1975 in Kwidzyn, Poland. He received M.Sc. degrees from the Gdansk University of Technology in 2000. At present, he is researcher at the Gdansk University of Technology. His field of interest are current limiters and computer analysis.

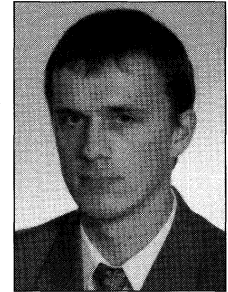
plesn@ely.pg.gda.pl



Mgr inż. Kazimierz GOHRA

He was born in 1972 in Puck, Poland. He received M.Sc. degrees from the Gdansk University of Technology in 1998. At present, he is researcher at the Gdansk University of Technology. His field of interest are partial discharge and electrical treeing.

kgohra@ely.pg.gda.p



Abstract

The paper presents operation of a hybrid contactless short-circuit current limiter on the basis of computer simulation. Special attention was paid to the possibility of improving of the quality of the delivered electrical energy, through limiting of the voltage dips duration in the power grid owing to the application of a hybrid circuit breaker. The calculations were performed using the PSPICE and MATLAB software.

Streszczenie

W artykule przedstawiono działanie bezstykowego ogranicznika prądów zwarciovych w oparciu o symulację komputerową. Szczególną uwagę zwrócono na możliwość poprawy jakości dostarczanej energii elektrycznej, poprzez ograniczenia trwania zapadów napięcia w sieci elektroenergetycznej, dzięki zastosowaniu wyłącznika hybrydowego. Modelowanie matematyczne wykonano w programie MATLAB i PSPICE.

Keywords: hybrid circuit breaker, voltage dip, contactless current limiter
Słowa kluczowe: łącznik hybrydowy, zapady napięcia, bezstykowy ogranicznik prądu

1. Introduction

In distribution systems the power quality is of increasing importance as the low voltage consumers use microelectronic components for control and operation, which are sensitive to voltage dips and power supply interruptions. Voltage dips can be defined as follows: a voltage dip is a sudden voltage reduction ranging from 1% to 90% of the nominal voltage and with a short circuit duration from 10 ms up to one minute [1]. In the US a short-duration reduction (up to a few seconds) in the voltage amplitude is termed a voltage sag [2].

Typically, voltage dips are due to short circuit faults in the power system. The time of disturbance elimination by classical contact circuit breakers is of several dozens milliseconds. It is too long to limit fault currents, and to reduce the duration of the voltage dip. Effective limitation of voltage dips can be achieved, among other means, by the application of hybrid circuit breakers [2].

One of the first hybrid circuit breakers put in the practice was designed by Collard and Pellichero [3]. Later on Żyborski [4] and Bartosik [5] significantly developed their idea. A modified approach was presented by Wolny [6] who applied a special ultra short fuse in the place of the contact switch. This way the need for a fast electrodynamic drive was eliminated, which allowed to considerably reduce dimensions and costs of the hybrid current limiter. The new device is called the contactless hybrid current limiter (CHCL).

Design of the analyzed CHCL

In fig. 1 the structure of the analyzed CHCL is presented. It consists of the following basic elements: the ultra short fuse (USF) shunted by the semiconductor device (SD), controlled by a special control

system (CS), and the metal oxide varistor (MOV) absorbing the magnetic field energy of the switched-off circuit. The triggering impulses may be controlled by the voltage across the USF.

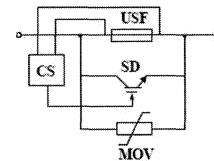


Fig. 1. The model of a hybrid DC switch [6]

Rys. 1. Model łącznika hybrydowego prądu stałego [6]

In fig. 2 the voltage and current traces of the CHCL operation are shown. The experiments were carried out in the oscillatory LC circuit at the frequency of 480 Hz and the prospective short-circuit current of 1.2 kA. The used frequency higher than 50 Hz increased the rate of current rise, essential for current limitation devices.

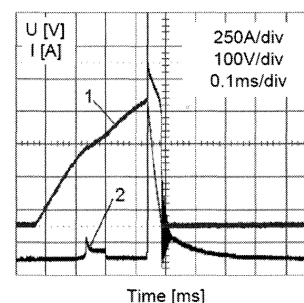


Fig. 2. The oscillograph records of the CHCL operation with an IGBT transistor; 1 - the CHCL current, 2 - the voltage

Rys. 2. Oscylogram działania CHCL z tranzystorem IGBT; 1 - prąd CHCL, 2 - napięcie

Modelling of CHCL operation

Due to the simulation of operation of a hybrid circuit breaker, a complex analysis of the components of a given assembly and its parameters is possible. In numerical experiments, a very important role is played by the proper selection of models of the components [7], of the analysed circuit. In simulations of the operation of a CHCL, the selection of the ultra short fuse arc model is a difficult and important issue, since due to the prevailing axial cooling no existing arc model can be directly applied. The calculations were performed using the PSPICE and MATLAB software.

In regard to the PSPICE simulations, the arc model was founded on a voltage-controlled switch modified by the application of a non-linear resistance connected in parallel to the opening contacts.

With regard to the MATLAB a ready-to-use model based on the Cassie's concept is offered [8]. However such a rough model did not work properly. Hence modification had to be introduced consisted in the addition of energy-absorbing elements connected in parallel to the arc. The resistance and capacitance were used.

Commercial programs offer a large selection of models of the semiconductor devices available on the market. The list is amended every time when a new device is developed. Different approaches of model selection are adopted in the MATLAB and the PSPICE. In the former case, parameters of a generic model of the device are modified in accordance to the actual catalogue data. In the case of the PSPICE ready-to-use models are only available.

The results of the numerical experiments, obtained with the PSPICE software are presented in fig. 3. The calculations were carried out in the oscillatory LC circuit at the frequency of 480 Hz and the prospective short-circuit current of 1.2 kA

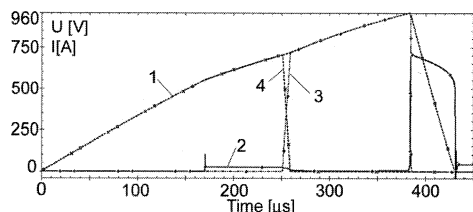


Fig. 3. The record of CHCL operation (PSPICE): 1-the switch current, 2- the switch voltage, 3 - the IGBT current, 5 - the fuse current

Rys. 3. Działanie CHCL (PSPICE): 1-prąd łącznika, 2 - napięcie, 3 - prąd tranzystora IGBT, 4 - prąd bezpiecznika

Similar results obtained in physical and numerical experiments (fig. 2 and fig. 3) allow for an analysis of the operation of a hybrid circuit breaker in an AC circuit with a frequency of 50 Hz.

The numerical experiment was performed with the MATLAB software. The simulation was performed for the circuit presented in fig. 4.

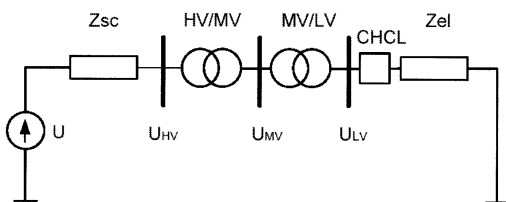


Fig. 4. The modelled power-system grid segment: U - the voltage source, Z_{sc} - the system impedance, HV/WV, MV/LV - the transformer, Z_{el} - the load impedance

Rys. 4. Modelowany fragment systemu elektroenergetycznego Modelowany fragment systemu elektroenergetycznego: U - źródło napięcia, Z_{sc} - impedancja systemu, HV/WV, MV/LV - transformator, Z_{el} - impedancja obciążenia

2. Effect of the semiconductor device control on the operation of a hybrid circuit breaker

In the operation of a hybrid circuit breaker an important problem is the proper control of the semiconductor device. Delayed turn-off causes an increase in the cut-off current, while in the case of an early turn-off, there is the possibility that the gap in the molten fuse element will be too short and will not withstand the recovery voltage. In fig. 5 the relationship between the shortest permissible IGBT time on and the arcing time of the short fuse are shown [9].

Durations of the fuse element melting and the increase in the recovery dielectric strength are associated with the cut-off current, while the recovery voltage, which must be withstood by the limiter, depends on the actual state of the power system. Any delay in the cut-off process is detrimental, as it increases the limited current, fault clearing time and the energy allowed through by the hybrid circuit breaker.

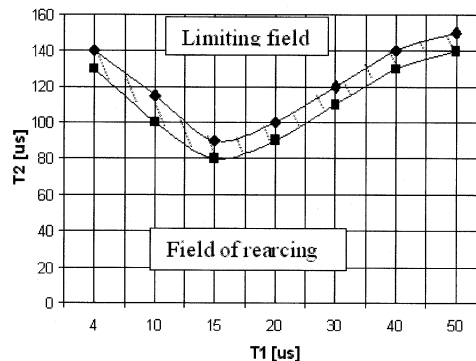


Fig. 5. The relationship between the shortest permissible IGBT time on and the arcing time of the short fuse; T1- arcing time, T2 - recovery time of the fuse dielectric strength [9]

Rys. 5. Zależność między czasem odbudowy wytrzymałości przerwy a czasem łukowym bezpiecznika; T1- czas łukowy, T2 - czas odbudowy wytrzymałości dielektrycznej przerwy [9]

Selection of the optimal making and cut-off moment of the semiconductor device is of great significance for the quality of the power supply. The shorter the duration of the short circuit fault, the shorter the duration of the voltage disturbance in the power system will be. However, selection of very short turn-on and let-through times of the IGBT will cause the arc reignition, and this way an increase in the duration of disturbance in the power delivery and the possibility of current limiter damage. In fig. 6 the elimination of a short circuit fault in the power system is presented, using a classical switch (1). The duration of the voltage dip is $\Delta t=31$ ms.

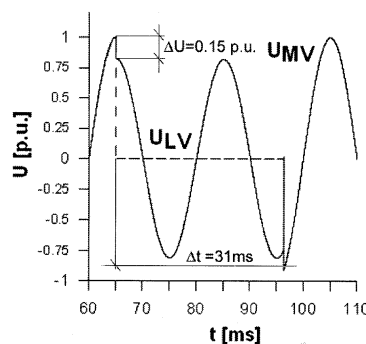


Fig. 6. Fault clearing time with a contact switch (simulation)

Rys. 6. Czas trwania zakłócenia w przypadku łącznika zestykowego (symulacja)

A considerable limitation of the disturbance duration is achieved using a hybrid circuit breaker. In this case, the time necessary to eliminate a disturbance depends, to a great degree, on the IGBT control delay. In fig. 7 the short circuit cut-off time using a hybrid circuit breaker is shown. In this case, the time necessary to eliminate a disturbance is $\Delta t = 0.9$ ms.

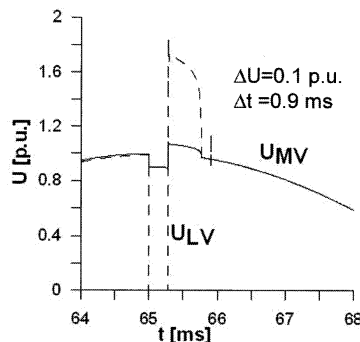


Fig. 7. Fault clearing time with the CHCL (simulation)

Rys. 7. Czas trwania zakłócenia w przypadku łącznika hybrydowego (symulacja)

However, the selection of the optimum current let-through time of the semiconductor device is a very complex issue. It should be as short as possible from the point of view of the quality of the supplied power. On the other hand, taking into consideration the current transfer requirements it must be long enough to allow for the disintegration of the fuse element and the recovery of dielectric strength of the fuse, in order to prevent the reignition.

3. Summary

The voltage dips disturb high quality power supply. They can cause identical results, as total interruption in the electrical energy supply, particularly dangerous for electronic devices, which are very sensitive to rapid voltage changes.

The voltage dips, due to short circuit faults in power system, can be reduced, by the application of the hybrid circuit breaker, whose fault-clearing time is merely a few hundreds of μ s.

The optimum control of the hybrid circuit breaker should consider:

- maximum limitation of the disturbance duration,
- minimization of the energy let-through by the current limiter during any fault occurrence.

The research on contactless current limiting device has been carried out in the frames of the current research project No: 8 T10A 058 21 financed by the Committee of Scientific Research in Poland.

References

[1] G. Brauner, Ch. Hennerbicher: Voltage dips and sensitivity of consumers in low voltage networks, CIRED, 18-21 June 2001.

[2] J. Żyboriski, A. Holc: Energy quality improvement by ultra rapid L.V. fault current limiting and interrupting, 10-th International Symposium on "Short Circuit in Power Systems", Lodz, 28-29 October 2002, Conf. Proc., p.243-248.

[3] P. Collart, S. Pellichero: A new high speed DC circuit breaker: the D.H.R., Colloquium Organized by Professional Group P6 and P2, London, 1989.

[4] J.Czucha, M. Pikoń, J. Żyboriski: Ultra rapid IGBT current limiting interrupting device of very high breaking capacity, 8th International Symposium on Short-Circuit Current in Power System, Brussels 1998, p.219-222.

[5] M., Batrosik F. Wójcicie: Arcless DC hybrid circuit breaker. SAP&ETEP-97, Lodz 1997.

[6] A. Wolny, B. Semenowicz: Hybrid contactless short-circuit current limitation, 10-th International Symposium on "Short Circuit in Power Systems", Lodz, 28-29 October 2002, Conf. Proc., p.221-225.

[7] P. Leśniewski, B. Semenowicz, K. Gohra: Influence of circuit parameters on the process of current transfer in the hybrid circuit breaker, XIII-th Symposium on Electrical Apparatus and Technologies SIELA 2003, 29-30 May, 2003, Conf. Proc. Vol. I,

[8] Schavemaker P.H.: "Arc model blockset for use with MATLAB Simulink and Power System Blokset - User's guide". Delft University of Technology, 2001.

[9] B. Semenowicz, R. Partyka: Dielectric strength of the ultra-short fuse, Seventh International Conference of Electric Fuses and their applications, 8-10 September, Jurata 2003.

Tytuł: Ograniczenie zapadów napięcia za pomocą bezstykowego ogranicznika prądu

Artykuł recenzowany

NOWE OBNIŻONE CENY REKLAM W PAK-u CENNIK PUBLIKACJI PŁATNYCH na I półrocze 2004 roku

REKLAMA	Czarno-biała	Kolorowa
*) I okładka	-----	3200 zł
II okładka	-----	2800 zł
III okładka	-----	2700 zł
IV okładka	-----	3000 zł
1 strona (175x225 mm)	1200 zł	1800 zł
½ strony (175x125 mm) - pozioma	700 zł	1050 zł
½ strony (85x225 mm) - pionowa	700 zł	1050 zł
¼ strony (85x125 mm)	450 zł	675 zł
***) ¼ strony (85x60 mm) - pozioma	250 zł	400 zł
*) dodatkowa informacja na okładce wg uzgodnień		
**) tylko wg indywidualnych uzgodnień		

ARTYKUŁY TECHNICZNO-INFORMACYJNE

Adresowane do specjalistów na poziomie inżynierskim

1 strona PAK - 1000 zł (+ 50% kolor)

Cena do uzgodnienia w zależności od liczby stron i sponsorowanego tematu

STAŁE WKŁADKI

tematyczne lub firmowe, wydrukowane przez zleceniodawcę

- 1-kartkowe (2-stronicowe) - 2000 zł
- 2-kartkowe (4-stronicowe) - 3000 zł
- wielokartkowe (do 12 stron) - 4000÷5000 zł

Do wszystkich cen doliczamy podatek VAT 22%