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# Exhaled breath gas sensing using pristine and functionalised

## WO<sub>3</sub> nanowire sensors enhanced by UV-light irradiation

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## **Abstract**

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The development of advanced metal-oxide-semiconductor (MOS) sensing technologies for the detection of volatile organic compounds (VOCs) present in the exhaled breath is of great importance for non-invasive, cheap and fast medical diagnostics. Our experimental studies investigate the effects of operating temperature selection and UV-light irradiation on improving the sensitivity of WO<sub>3</sub> nanowire sensors for exhaled breath exposure. Herein, six WO<sub>3</sub> nanowire sensors (both pristine and doped with a range of metal nanoparticles such as Pt, Au, Au/Pt, Ni and Fe) were synthesised via aerosol-assisted chemical vapour deposition (AACVD) and characterised by means of atomic force microscopy (AFM), scanning electron microscopy (SEM), transmission electron microscopy (TEM) and energy dispersive X-ray (EDX-ray). Breath measurements were performed in the dark and under UV-light irradiation at various sensor operating temperatures. The results demonstrate that UV-light irradiation combined with the optimisation of the sensors' operating temperature can greatly enhance the sensors' responses towards breath exposure.



## **Keywords**

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- 37 WO<sub>3</sub> nanowire sensors, metal nanoparticles, sensitivity enhancement, UV-light irradiation,
- 38 operating temperature, exhaled breath analysis.

## 1. Introduction

Exhaled breath is a valuable, non-invasive biological tool available for diagnosing and monitoring medical conditions (Gardner et al., 2000; Adiguzel & Kulah 2015; Lentka et al., 2016; Saidi et al., 2018). Its popularity in medicine can be demonstrated by an increase in papers published in this area. Therefore, the development of advanced and cheap sensors of high sensitivity towards low concentrations of VOCs in the exhaled breath is of paramount importance. In this regard, MOS chemical gas sensors have emerged as a very promising tool for monitoring low concentrations of gaseous compounds (Konvalina & Haick 2014; Welearegay et al., 2016; Zhang et al., 2017), and they represent a low-cost alternative as compared to other available analytical methods (e.g., Gas Chromatography/Mass Spectrometry) that require expensive and bulky equipment. Tungsten trioxide (WO<sub>3</sub>), with a band gap of about 2.8 eV (Yun et al., 2016), is one of the most important n-type MOSs, and it has been extensively used as a gas sensor material for VOC detection (Righettoni et al., 2010; Choi et al., 2014; Kim et al., 2016;

Shendage et al., 2017). However, its selectivity and sensitivity are still too low for some applications, such as breath analysis. The selectivity can be partially improved by using a set of sensors with different cross-sensing performances and enhanced by reducing the particle size to a range of 5 to 50 nm (Yamazoe, 1991; Shimizu and Egashira, 1999; Ederth at al., 2006). Alternatively, the sensing potential of WO<sub>3</sub> sensors can be significantly improved by doping the sensing layer with a small amount of metal nanoparticles (NPs), such as platinum, gold, nickel, iron, etc. (Vallejos et al., 2013; Ahsan et al., 2013; Vilic and Llobet 2016). Metal doping



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is considered a crucial option for diversifying the selectivity and improving the sensitivity of 60 the sensors. Nevertheless, the sensing performance of the WO3 sensors must be further 61 62 optimised to satisfy the requirements for breath analysis applications.

WO<sub>3</sub> NW sensors generally operate at elevated temperatures because the detection mechanisms are based on thermo-activated chemical reactions between the sensing film and the adsorbed VOCs (Bendahan et al., 2007). Variation of the sensor's operating temperature may enhance its sensitivity (Paulsson and Winquist, 1999; Taurino et al., 2002; Ionescu and Llobet 2002; Zhang et al., 2015). Besides, many researchers have proven that WO<sub>3</sub> sensor performance could be influenced by a photocatalytic effect such as UV-light irradiation (Iliev et al., 2010; Giberti et al., 2012; Smulko et al., 2015; Trawka et al., 2016; Gonzalez et al., 2016). The sensitive film of the sensor absorbs the UV-light (Mishra et al., 2004), which provides a further dissociation of the gaseous compounds and the consequent molecule adsorption (Trawka et al., 2016). UV-light irradiation creates a charge transport that increases the density of free electron-hole pairs (Karaduman et al., 2014; Xu et al., 2015). Therefore, it alters the sensing layer. Moreover, the applied UV-light of selected wavelengths can modulate the sensing properties in a different way due to various penetration depths, related to the applied wavelength and morphology of the porous gas sensing layer. Altogether, the response of MOS gas sensors can be successfully modified by UV-light that reduces the necessary heating energy (Park et al., 2013; Espid and Taghipour, 2017).

In our paper, pristine and metal-doped WO<sub>3</sub> NWs were elaborated using aerosol-assisted chemical vapour deposition (AACVD) and characterised by using Atomic Force Microscopy (AFM), Scanning Electron Microscopy (SEM), Transmission Electron Microscopy (TEM) and Energy Dispersive X-ray (EDX-ray). The effects of UV-light irradiation and operating temperature selection were investigated regarding the analysis of exhaled breath.



## 2. Materials and methods

#### 2.1. Sensor fabrication

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AACVD was used to grow WO<sub>3</sub> NWs due to its simplicity and relatively low temperature experimental conditions (Annanouch et al., 2013; Qadri et al., 2016). This method consists of delivering a suitable precursor in the form of an aerosol into the reactor where the substrate is mounted (Stoycheva et al. 2012). In our study, six different sensors (i.e., pristine WO<sub>3</sub> NWs and the following pool of metaldoped WO<sub>3</sub> NWs: Pt/WO<sub>3</sub>; Au/Pt/WO<sub>3</sub>; Au/WO<sub>3</sub>; Ni/WO<sub>3</sub>; and Fe/WO<sub>3</sub>) were grown using AACVD. Alumina substrates with Pt interdigitated electrodes on the front-side and a Pt meander heater on the back-side were employed as sensing substrates from CeramTec© (Marktredwitz, Germany). The substrates were successively cleaned with ethanol, acetone and distilled water and dried with a nitrogen flow before they were placed inside the AACVD reactor. The layers of WO<sub>3</sub> NWs were prepared using tungsten hexacarbonyl (WC<sub>6</sub>O<sub>6</sub>) as a precursor according to previous reported procedures (Annanouch et al., 2015; Thamri et al., 2016). The experimental conditions for growing the six sensors are provided in Table 1. After nanomaterial synthesis, the deposited films were annealed in an oven (Carbolite's calcination furnace 1200 °C | BWF) at 500 °C for 180 minutes under a constant flow of 200 mL/min of synthetic air. This step was carried out in order to clean the surface of deposition residues and to stabilise and crystallise the structure of the grown nanomaterials (Stankova et al., 2005; Ng et al., 2015). Otherwise, the morphology and composition of the deposited films were characterised. SEM measurements were performed using a FEI-ESEM Quanta 600 equipment (20 keV), which was coupled to an EDX analyser from Oxford Instruments. A TEM analysis of the

Nanoparticles' sizes was done by JEOL JEM-1011 equipment with an accelerating energy of



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100 keV while the structure of the deposited film was studied with AFM by means of a Keysight 5500 SPM.

AACVD reaction of WC<sub>6</sub>O<sub>6</sub> with a mixture of acetone and methanol, inside a hot wall reactor, resulted in the formation of blue-black WO<sub>3</sub> films. Applying the annealing process on these films at 500 °C yielded yellow layers that indicated fully oxidised WO<sub>3</sub>. AFM analysis was used in acoustic mode to assess a topography of the annealed surface of the deposited layers. Figure 1 presents orthogonal 3D images of the AFM topography of pristine and functionalised WO<sub>3</sub> films deposited onto alumina substrate which is scanned within an area of 10 µm<sup>2</sup>. It can be seen that the maximal heights of the pristine WO<sub>3</sub> and Fe/WO<sub>3</sub> NWs were 2.2 µm and 3.4 nm, respectively (Fig. 1.a, Fig. 1.f). However, a significant reduction of surface roughness was achieved by functionalising the sensing surface with metal nanoparticles (except for Fe nanoparticles). Maximal heights of 762 nm, 713 nm, 991 nm and 505 nm for Pt/WO<sub>3</sub> (Fig. 1.b), Au/Pt/WO<sub>3</sub> (Fig. 1.c), Au/WO<sub>3</sub> (Fig. 1.d) and Ni/WO<sub>3</sub> (Fig. 1.e) were obtained, respectively. In all cases, AFM images showed complete coverage of the WO<sub>3</sub> films on the entire substrate surface. It seems that the shape of the grains varied when changing the catalysts. Figure 2.a shows a typical SEM image of the pristine WO<sub>3</sub>. It can be seen that the AACVD method at 500 °C produced a layer of thick NWs (about 159 nm), with high density and quite a homogeneous distribution on the entire substrate. In contrast, the films that contain Pt and/or Au Nps exhibited a mixture of randomly distributed nanowires with a diameter ranging between 45 and 57 nm (Fig. 2.b, Fig. 2.c and Fig. 2.d). The layer of Ni/WO<sub>3</sub> showed high density NWs which were randomly distributed (Fig. 3.e). SEM data of Fe/WO<sub>3</sub> also show NWs of various sizes with a diameter ranging between 47 and 126 nm (Fig. 2.f). The AACVD yields a high density of non-aligned nanowires, with a relatively homogeneous distribution containing small pores over the studied surfaces. TEM of the deposited layers for pristine and functionalised WO<sub>3</sub> displayed porous polycrystalline films in thinner structures, approximately as spherical or



cylindrical morphologies (Fig. 3). Nanowires and nanoparticles can be easily observed from the recorded images. They appear well dispersed along the surface of the WO<sub>3</sub> films. The grain diameters of the studied metal Nps were about 11 nm for Pt Nps (Fig. 3.b), 4.63 nm for the alloy of Au/Pt Nps (Fig. 3.c), 3.97 nm for Au Nps (Fig. 3.d), 39 nm for Ni Nps (Fig. 3.e) and 8.22 nm for Fe Nps (Fig. 3.f). The results show that the set of the investigated sensors was characterised by their high surface-to-volume ratio, which provides more surface area for both chemical and physical interactions and therefore secures better sensitivity. The EDX spectrum (Fig. 4) showed tungsten, oxygen and alumina (from the substrate) as the major peaks, and also revealed the presence of metal nanoparticles on the surface of the sensing nanomaterials. The percentages of metal nanostructures on the sensing films varied between 1% and 2% except for Pt Nps where it is found within 6% to 7% due to presence of platinum connectors to the substrate.

#### 2.2. Measurement set-up and conditions

The main part of the presented experimental studies required a collection of exhaled breath samples. To avoid any eventual artefacts, the breath samples were taken from the same individual (non-smoker, adult man) using Tedlar® bags before any food or beverage consumption. For this, the person took a deep breath, and breathed normally into the collection bag before empting his lungs. The breath sample was immediately transferred from the collection bag into the gas chamber where the sensors were placed. This was done by pumping the contents of each filled bag at a constant flow rate of 100 mL/min.

The experiments began by starting a flow of current through the sensors' heaters, corresponding to the selected temperature, for 1000 s. Next, the sensors were exposed to the collected breath sample for 40 min, and ended with the next 80 min of recovery under laboratory air using the same flow rate of 100 mL/min. An exposure of the sensors' to the exhaled breath was done both in dark and under UV-light irradiation. The sensors' conductance was continuously recorded at

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a sampling rate of 1 Hz using an NI USB-6212 data acquisition board from National Instruments (Texas, USA). The sensors' conductance was determine by measuring the DC voltage across the sensor as part of a voltage divider with another resistor connected in series and supplied by a DC voltage of 5 V. Figure 5 shows the circuit of the electrical current control unit for the heaters of three sensors. This unit was repeated to supply DC current for the next three heaters. The operating temperature was controlled by choosing the resistances of the heaters (RHn,  $n = 1 \dots 6$ ) with a selected current, adjusted by a potentiometer (P). The experiment was performed using an array of six independent sensors in the dark and under UV-light irradiation emitted by six OSV4YL5451B type diodes from *Opto-Supply*, China. Each diode was mounted above the sensor at the same distance, and the optical power irradiating the gas sensing layer was similar for each sensor.

The relative humidity and temperature inside the gas chamber was monitored during the experiment with a HIH 4000-002 humidity sensor from Honeywell, USA, and a LM35DZ temperature sensor from Texas Instruments, USA. The stability of the relative humidity  $(28\% \pm 5\%)$  and temperature  $(40^{\circ}\text{C} \pm 1^{\circ}\text{C})$  were recorded.

## 3. Results and discussion

Firstly, an experimental study was performed to find the most suitable operating temperatures of the sensors that secured the best responses to exhaled breath samples. It was found that each sensor has a range of operating temperatures, usually between 90°C and 120°C for pristine WO<sub>3</sub>, Pt/WO<sub>3</sub> and Au/Pt/WO<sub>3</sub> sensors (Subset #1), and between 140°C and 200°C for Au/WO<sub>3</sub>, Ni/WO<sub>3</sub> and Fe/WO<sub>3</sub> sensors (Subset #2). We selected temperature ranges to include the optimal operating temperature for both sensor batches when exposed to breath samples.

Figure 6 shows the sensors' responses towards two successive breath exposures in the dark (blue curves) and under UV-light irradiation (red curves); the sensors from Subset #1 operated



at 100 °C (Fig. 6.a, Fig. 6.b, Fig. 6.c), and the sensors from Subset #2 at 160 °C (Fig. 6.d, Fig. 6.e and Fig. 6.f). Importantly, it can be seen that the sensors' responses became relatively more intense under UV-light irradiation than in the dark. This effect can be measured by a quotient Q of two conductances:

$$Q = \frac{G_{F_{UV}}}{G_{F_{dark}}} \times 100\% \tag{1}$$

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- $G_{F_{LUV}}$  conductance observed after breath exposure under UV-light at the final stage of the experiment,
  - $G_{F\_dark}$  conductance observed after breath exposure in the dark at the final stage of the experiment.

The quotient Q reached at least 150%. For the pristine WO<sub>3</sub> NW sensor, it reached Q = 323%. This result is associated with the photocatalytic reactions taking place in the sensing film and with decomposition of the breath VOCs that are then adsorbed by the sensing material (Trawka et al., 2016). When the photons' energy overtakes the energy band gap  $E_g$  of the semiconductor, a generated electron (e<sup>-</sup>) in the valence band is excited into the conduction band, leaving a positive hole (h<sup>+</sup>) in the valence band (Wu et al., 2015). The energy gap of WO<sub>3</sub> is  $E_{\rm g} \approx 2.8 \; {\rm eV}$ , whereas the UV LEDs' wavelength is 394 nm, corresponding to a photon energy of 3.15 eV. As a photon's energy emitted from the UV LEDs is higher than the energy gap for WO<sub>3</sub> material, the sensor's conductance under UV-light irradiation should depend on the interband transitions (Giberti et al., 2012).

When the sensors operated under UV-light irradiation, their responses were repeatable and their recovery time was relatively short (Fig. 6). When the sensors operated under dark conditions, their responses were much longer and exceeded the observation time. We can claim that the use



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of UV-light irradiation accelerated the desorption rate of the VOCs adsorbed by the sensing film before we switched to only the laboratory air. At the same time, UV-light quickened the saturation of the investigated sensors when exposed to VOCs.

Figure 7 displays the responses to breath exposure of three investigated sensors operating at selected temperatures. The presented data proves that under UV-light irradiation, the sensors provide more repeatable responses and with more intense relative changes of conductance as compared to their operation under dark conditions. This effect may be explained by intensified desorption in the presence of UV light which accelerates cleansing of the sensors after breath exposure. We have noticed that an increase of the sensor's operating temperature quickened its response but decreased its relative changes of conductance. Thus, for the pristine WO<sub>3</sub> NW sensor, the UV/dark ratio (see Eq. 1) increased from 342% at 90 °C to 419% at 110 °C (when the sensor had not reached saturation during the experiment). At an operating temperature of 120 °C, the sensor response in the dark (blue curve) was more intense than at lower temperatures, and therefore the UV/dark ratio of conductances decreased to 212% (Fig. 7.a, Fig. 7.b and Fig. 7.c). In the case of the Au/Pt/WO<sub>3</sub> sensor, an operating temperature of 90 °C was too low to observe saturation or full recovery during the time of the experiment. The sensor started to saturate at a temperature of 110 °C both in the dark and under UV-light operation. UV-light irradiation assured a faster response, requiring only a few minutes, when compared to dark conditions, requiring about 30 min (Fig. 7.d, Fig. 7.e). For this sensor, again, the operating temperature of 120 °C assured more intense relative changes of conductance under dark conditions than at lower temperatures (Fig. 7.f). This is also observed for the Au/WO<sub>3</sub> sensor at different operating temperatures. This sensor (Subset #2), showed that at an operating temperature of 140 °C, saturation cannot be achieved in the dark nor under UV-light (Fig. 7.g). Full saturation at an operating temperature of 180°C is reached after about 30 min of breath exposure in the dark and after about 15 min under UV-light (Fig. 7.h). As a consequence,



the coefficient Q decreased from 333% at 180 °C to 181% at 200 °C (Fig. 7.i). These results suggest that the presence of metal NPs on WO<sub>3</sub> NW surfaces could seriously improve the sensor's sensitivity to exhaled breath exposure, while reducing its optimal operating temperature.

Based on the time of response, operating temperature of the investigated sensors and relative change of DC resistance, we may determine their sensitivity to the exhaled breath. Sensitivity S can be defined as a relative change of conductance  $G_F$  measured at the end of observation time (final conductance) in the ambient atmosphere of the exhaled breath and under dark conditions or UV-light irradiation (by using the index "dark or UV") and referenced to G measured in the ambient atmosphere of laboratory air:

$$S = \frac{G_{F (dark or UV)} - G_{0 (dark or UV)}}{G_{(dark or UV)}} \times 100\%$$
 (2)

All six sensors exhibited greater sensitivity when measured under UV-light irradiation at the investigated operating temperatures. Subset #1 of the sensors (pristine WO<sub>3</sub>, Pt/WO<sub>3</sub> and Au/Pt/WO<sub>3</sub>) reached higher sensitivities towards breath exposures at 100 °C both in the dark and under UV-light irradiation (Fig. 8.a, Fig. 8.b), which drastically decreased at 110 °C and further at 120 °C under UV-light irradiation. In the case of the sensors from Subset #2 (Au/WO<sub>3</sub>, Ni/WO<sub>3</sub> and Fe/WO<sub>3</sub>), their sensitivity changed slightly at the considered operating temperatures and in the dark (Fig. 8.c), while under UV-light irradiation, the changes were much more intense and the greatest sensitivity was observed at 160 °C (Fig. 8.d). The most significant difference between the sensitivity in the dark and under UV-light irradiation was found for the Au/WO<sub>3</sub> sensor, which increased from 88.9 % to 216.9% at 160 °C.

The reported results mean that a proper combination of the sensors' heating and UV-irradiation may play a crucial role in enhancing MOS WO<sub>3</sub> sensors' sensitivity towards the detection of

the VOC's in the exhaled breath. Their functionalisation by metal-doped nanoparticles is also important to determine the sensors' optimal operating temperature, together with the sensors' sensitivity and selectivity.

## 4. Conclusions

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Our experimental study presents the first ever report of UV-irradiation combined with a selection of the sensors' operating temperatures to enhance exhaled breath detection by WO<sub>3</sub> NW sensors decorated by selected metal dopants. The study was performed on both pristine and NP-doped WO<sub>3</sub> NWs grown by AACVD on alumina substrates and characterised by AFM, SEM, TEM and EDX-ray. All sensors clearly responded to the exhaled breath, both in the dark and under UV-light irradiation. In addition, their responses were repeatable and determined by their operating temperatures. The experimental results revealed that the most sensitive sensor towards the exhaled breath samples was the Au-doped WO<sub>3</sub> NWs operating at 160 °C. It reached a sensitivity as high as S = 216.9% under UV-light irradiation. These promising results may be a way for further development of low-cost, low-power consumption and highly sensitive gas sensors for medical applications.

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## Highlights

- AACVD was carried out to produce pristine and differently functionalised WO<sub>3</sub>
- The grown sensors were characterised with AFM, SEM, TEM and EDX-ray
- UV-light irradiation enhanced the sensors' responses towards breath exposure
- The most sensitive sensor for breath was the Au-doped WO<sub>3</sub> and operating at 160 °C

Figure 1 AFM topographies of the sensors' surfaces of: (a) pristine WO<sub>3</sub>; (b) Pt/WO<sub>3</sub>; (c) Au/Pt/WO<sub>3</sub>; (d) Au/WO<sub>3</sub>; (e) Ni/WO<sub>3</sub>; (f) Fe/WO<sub>3</sub>.

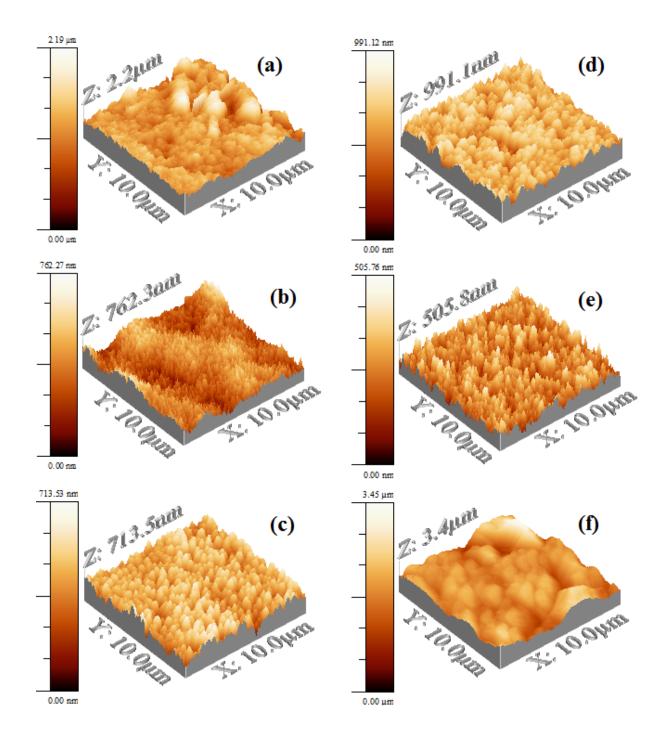




Figure 2 Typical SEM images of sensing areas of: (a) pristine WO<sub>3</sub>; (b) Pt/WO<sub>3</sub>; (c) Au/Pt/WO<sub>3</sub>; (d) Au/WO<sub>3</sub>; (e) Ni/WO<sub>3</sub>; (f) Fe/WO<sub>3</sub>.

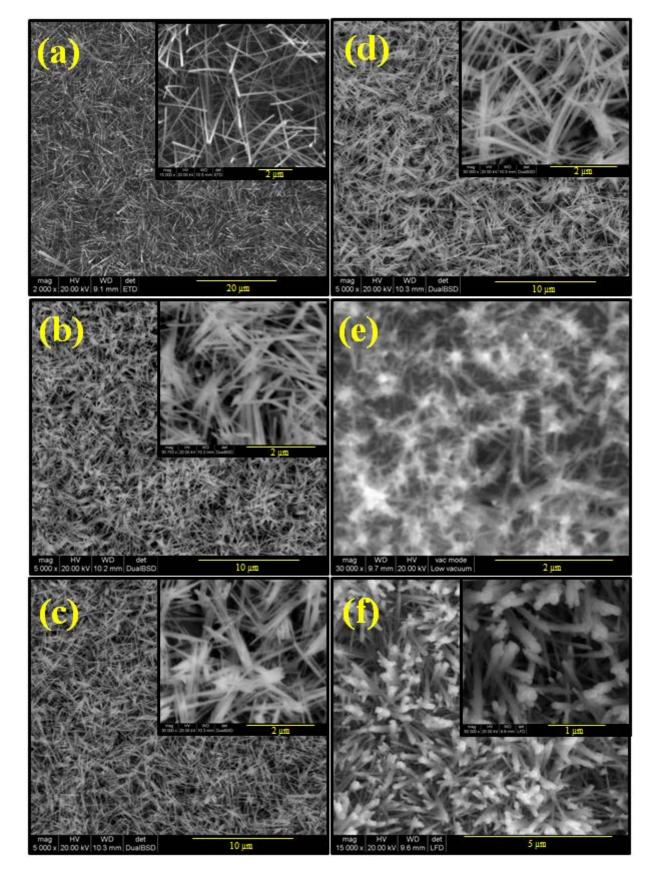




Figure 3 TEM images of the sensitive films of: (a) pristine WO<sub>3</sub>; (b) Pt/WO<sub>3</sub>; (c) Au/Pt/WO<sub>3</sub>; (d) Au/WO<sub>3</sub>; (e) Ni/WO<sub>3</sub>; (f) Fe/WO<sub>3</sub>.

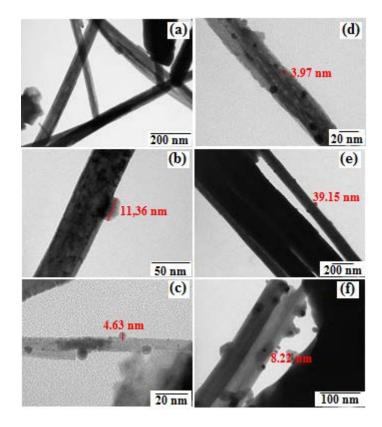




Figure 4 EDX-ray spectrum of the six sensors: (a) pristine WO<sub>3</sub>; (b) Pt/WO<sub>3</sub>; (c) Au/Pt/WO<sub>3</sub>; (d) Au/WO<sub>3</sub>; (e) Ni/WO<sub>3</sub>; (f) Fe/WO<sub>3</sub>.

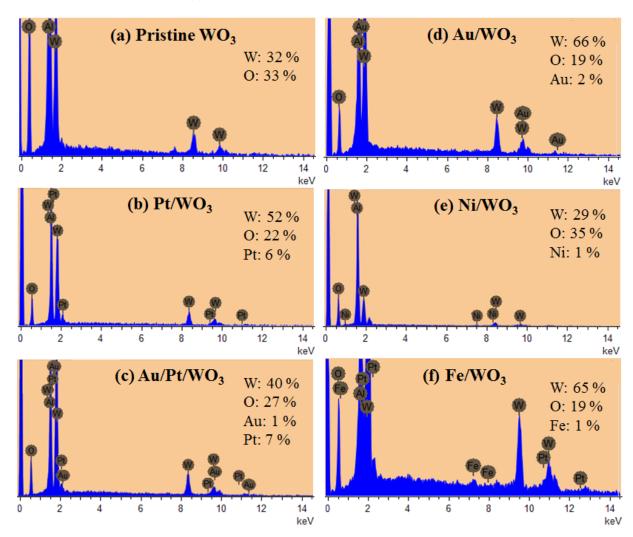




Figure 5 Electronic conditioning circuit for monitoring the current of three sensors' heaters connected in series.

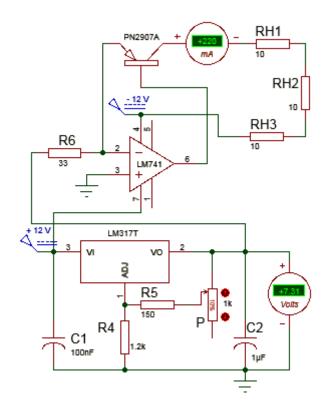




Figure 6 Sensors responses towards two repeated breath exposures in the dark (blue curves) and under UV-light illumination (red curves) for: (a) Pristine WO<sub>3</sub>; (b) Pt/WO<sub>3</sub>; (c) Au/Pt/WO<sub>3</sub>; (d) Au/WO<sub>3</sub>; (e) Ni/WO<sub>3</sub>; (f) Fe/WO<sub>3</sub>. Sensors (a) to (c) were operated at 100 °C, and sensors (d) to (f) at 160 °C.

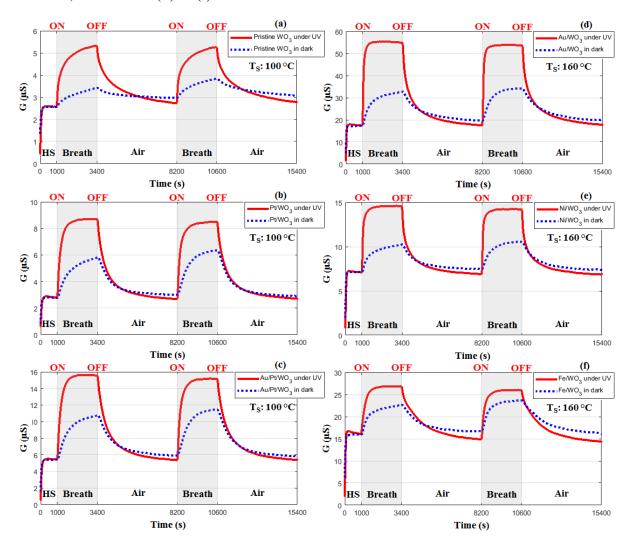




Figure 7 Sensors responses towards two repeated breath exposures in the dark (blue curves) and under UV-light illumination (red curves) for Pristine WO<sub>3</sub> sensor operated at: (a) 90 °C; (b) 110°C; (c) 120 °C; Au/Pt/WO<sub>3</sub> sensor operated at: (d) 90 °C, (e) 110°C; (f) 120 °C; Au/WO<sub>3</sub> sensor operated at: (g) 140 °C; (h) 180 °C; (i) 200 °C.

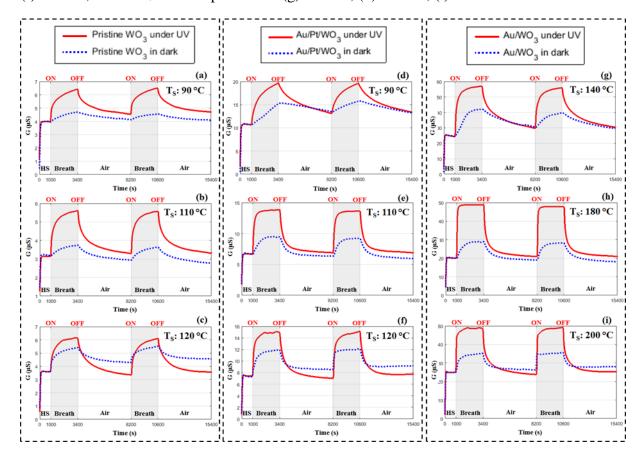




Figure 8 Sensors sensitivities in the presence of breath exposure at four different temperatures for pristine WO<sub>3</sub>, Pt/WO<sub>3</sub>, Au/Pt/WO<sub>3</sub>: (a) in dark, (b) under UV irradiation; and Au/WO<sub>3</sub>, Ni/WO<sub>3</sub>, Fe/WO<sub>3</sub>: (c) in dark, (d) under UV irradiation.

